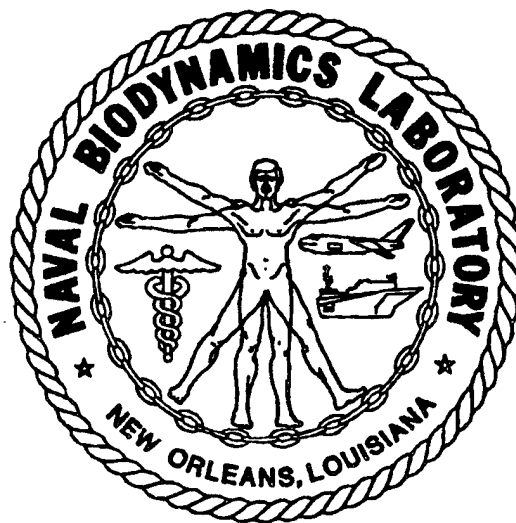


**DYNAMIC VARIABLE AND TEMPORARY INJURY CORRELATION
FOR HUMAN HEAD AND NECK IMPACT EXPERIMENTS**

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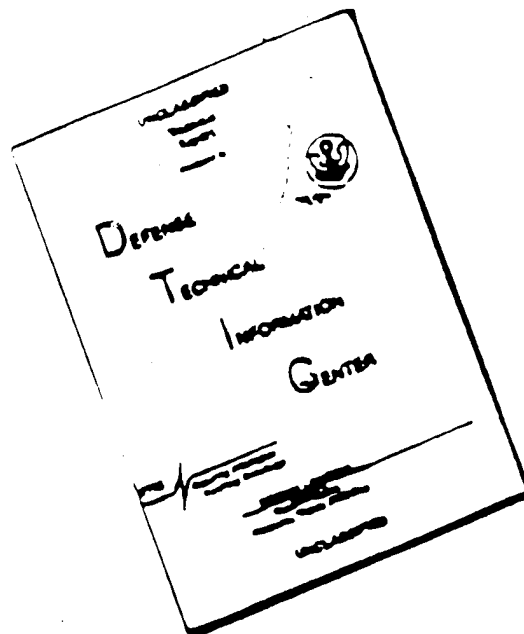
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DYNAMIC VARIABLE AND TEMPORARY INJURY CORRELATION FOR HUMAN HEAD AND NECK IMPACT EXPERIMENTS

BRIAN W. WAMSLEY, ALVAH C. BITTNER, JR., NORMAN S. GILBERT,
LEONARD S. LUSTICK

ABSTRACT

The Naval Biodynamics Laboratory (NBDL) has collected a data base describing the head/neck kinematic response of a large number of human subject volunteers to -X, +Y, and -X+Y vector exposures. This paper will present injury-related parameters for the most severe exposures in each vector, together with correlations of these parameters with the medical findings. The parameters presented include axial and shear forces and torques at the occipital condyles, as well as the head injury criterion (HIC number). Moderate ($R = .35$ and $.38$) but highly significant ($p < .025$) correlations were revealed between general (GENFAC) and muscle (MUSFAC) symptom factor variables. These findings encourage continued systematic evaluation of the relationship between the observed injury-related (eg. axial and shear) and medical findings.

INTRODUCTION

The Naval Biodynamics Laboratory (NBDL) has collected a data base describing the head-neck kinematic response of human subject volunteers to -X, +Y, and -X +Y, vector exposures. The goal of this program has been to develop human dynamic and injury response models to impact acceleration as well as to determine the correlation of dynamic responses with physiological effects and injuries. This information is in use for design, construction, and validation of manikins and mathematical models. These products are used to evaluate human protective systems for prevention of casualties from severe impacts (e.g., aircraft crashes and ejections). Thomas, Ewing, Majewski, and Gilbert (1) have previously reported modest correlation between clinical medical effects and sled acceleration and direction. Interestingly, current as well as previous modeling efforts predict that such correlations would be greater, if correlations were made relating "injury-related variables" (eg., maximum shear) with clinical variables (eg., Ewing et al. (2) and Muzzy et al. (3)). This paper will present injury-related parameters for maximum -X,+Y, and -X+Y exposures and their correlations with medical findings.

METHOD

Subjects--The subjects were six Navy enlisted men (ages 19 to 23) who had volunteered for duty as biodynamics research subjects (ie., subjects H131 to H136). They had been selected to be unusually free of skeletal, cardiopulmonary and other medical or psychological conditions which would preclude participation in potentially hazardous environmental research. The subjects were otherwise typical of the general enlisted population. All subjects were recruited, evaluated, and employed in accordance with SECNAV Instruction Series 3900.39 and MANMED Instruction Series 3900.6.



These instructions are based upon informed voluntary consent and meet the provisions of prevailing national and international guidelines regarding proper human experimentation. A more detailed description of the volunteers and their selection is given by Thomas, Majewski, Ewing, and Gilbert (4). Tables 1 and 2 respectively contain selected measured and estimated anthropometric parameters for the volunteer subjects.

ABSTRACT

Tables 1 and 2 about here

Experimental Design -- Subjects were exposed sequentially to blocks of $G(-x)$, $G(+y)$ and $G(-x+y)$ sled profiles with respective maximums of 15, 7 and 9Gs. To minimize the effects of initial conditions each subject was always run in the neck-up, chin-up condition which is standard at NBDL (Ewing et al. (5)). Subjects were medically examined by a physician immediately prior to, shortly after, and 24 hours postrun (or until the abatement of any significant medical findings). This information was recorded for later computer analysis. Retrospective review of the post run medical log yielded five categories of symptoms and physical findings in keeping with that reported by Ewing et al (2). These were (1) hours of muscle soreness; (2) hours of muscle stiffness; (3) hours of headache; (4) hours of backache, and (5) other.

Apparatus -- A Bendix Hyge(R) pneumatically driven .3048m diameter accelerator was used to accelerate an approximately 1.2m by 3.7m multivectorial sled which was rail mounted on Delrin AF(R) pucks. The acceleration stroke is limited to 1.52m and sled mounted brakes were not used. The effective drag is about .2G and the sled was allowed to coast to a stop. Total rail length available is 213m. The impact direction ($-X$, $+Y$ or $-X+Y$) was determined by rotation of the multivectorial sled.

The subjects were restrained in a nominally upright position by shoulder straps, a lap belt and an inverted "V" pelvic strap tied to the lap belt. Upper arm and wrist restraints were used to prevent flailing. Figure 1 illustrates the basic restraint system which was used for the three vector directions.

Figure 1 about here

Experimental Measurements -- The dynamic variables presented in this paper were derived by integrated accelerometer and cinephotographic measurement systems (Seemann and Lustick, (6)). The accelerometer system yielded measurements using nine piezoresistive accelerometers mounted on a "T" shaped plate at the mouth and six accelerometers mounted on a T-plate at the spinous process of the first thoracic vertebral body (T(1)). The configuration of the accelerometers on the T-plate and the error propagations associated with this method for determining linear displacement, velocity, acceleration and angular orientation, angular velocity and angular acceleration components of a rigid body have been described (Becker and Willems, (7)). The cinephotographic system with the accelerometer system has been previously described (Becker, (8)).



In order to compare subjects at similar points in the anatomy, it is required to define a head anatomical coordinate system and a T(1) anatomical coordinate system (Thomas, (9)). These anthropometric coordinate systems are related to the instrumentation coordinate systems by three-dimensional x-ray anthropometry on each subject (Ewing et al. (5)).

estimated anthropometric parameters for the subjects.

One reference frame for the entire series of experiments is fixed to the laboratory. This is established by first defining a sled coordinate system in which the origin is a benchmark permanently machined into the sled structure. The +X axis is parallel but in the opposite direction to the thrust vector of the accelerator. The +Z axis is parallel to gravity and positive upward and the +Y axis is established so that the axes form an orthogonal right-hand system. A second frame of reference is fixed to the anatomical axes of the head as illustrated in figure 2. (cf Thomas, (9) for more detail). Both coordinate systems used in this study are right handed where X, Y, and Z axes are taken in that order.

any significant medical symptoms. This information was reported to the subject and the physician.

Figure 2 about here

and report of the physician.

The subject will also be required to report any symptoms.

Injury-related variables which will be tabularly reported for all runs include maximum and minimum:

>Linear force components (relative to head X, Y, and Z) over a sled run at the head-neck junction (condyles).

A multivectorial sled which was rail mounted on a sled.

>Torque components (around the head X, Y, and Z) and resultant forces at the head-neck junction.

and

>HIC component and resultant value for window widths of less than 200

seconds.

and

and

In addition, plots comparing the time course for these variables for the subjects with the greatest and smallest head mass parameter (H132 and H135) will be provided for illustration of the range of responses. Time courses for these and other selected variables will be graphically provided for a typical subject (H134). Only linear and torque force components will be related to the medical log symptoms by correlational analysis.

RESULTS

and

Evaluation of the data was conducted in three phases. During the first phase, dynamic variables believed to be injury-related were examined. Medical variables were analyzed during the second phase. The third phase was concerned with correlation of the injury-related variables and medical variables.



Injury-Related Variables.

Injury-related dynamic variables were tabulated and graphically analyzed during this phase of evaluation. Graphical analysis revealed, as might be expected that the injury-related variables tended to increase in magnitude with increasing exposure (G) levels for the three vector directions. Figures 3, 4, and 5 illustrate time courses for respective changes in the resultant force, resultant torque and HIC variables for a range of 10.2 to 15.6 G(-X), 5.3 to 7.0(+Y), and 9.3 to 11.4(-X+Y). It should be pointed out that occasionally, experienced forces may be substantially greater for a relatively lower sled G level than at higher levels for the same subject (e.g., H132 at 13 vs. 15 G(-x) in Appendix A). The trend toward increasing injury-related magnitudes with increased exposure limits focused our attention toward the higher levels in later analyses.

Figures 3, 4, and 5 about here

Graphical analyses also indicated that individual differences play a role in experienced forces under nominally the same sled force conditions. Figures 6, 7, and 8 show shear and axial forces as well as resultant torque time-courses for subjects with greatest (H135) and least (H132) head mass parameters. Over nominal 15G(-x), 7G(+y) and 10G(-x+y) conditions, the largest headed subject (H132) tended to experience greater stresses than the smallest subject. The larger subject, as will be seen later, also reported greater medical problems post-run. The apparent role of individual differences focused our attention on their importance in later analyses.

Figures 6, 7, and 8 about here

The results of graphical analysis suggested tabulating experienced injury-related variables for the greatest experienced level for each vector and each subject. The appendix contains a portion of this tabulation.

Medical Variables

The medical variables were tabulated and analyzed during the second phase of evaluation. Table 3 provides the basic data by subject and run. Examining this table, it may be noted that some runs were uneventful while other runs resulted in clusters of symptoms (muscle soreness and muscle stiffness tend to go together). It may also be seen that about 30 percent of the impact runs resulted in some significant symptom. The nature and frequency of such findings were similar to that reported by Thomas et al. (1) where significant symptoms were reported for about 40 percent of the runs. This clustering of symptoms suggested condensing the symptoms into "factors" which are more syndrome in character.

Table 3 about here.



A principal factor analysis was conducted on transformations of the variables shown in Table 3. The first four variables (hours of muscle soreness, through hours of backache) were transformed ($\log(x)+1$) to reduce skewness and theoretically enhance linearity. The last variable was coded as "0" or "1" to respectively denote the absence or presence of other symptoms. The transformed variables are subsequently labeled MUSOR, MUSIF, HEAD, BACK, and OTHER for purposes of identification. The analysis resulted in evidence of a strong first factor (syndrome) which accounted for 50.8% of the variance across the symptoms (eigen-value of 2.53). A second factor (syndrome) was also suggested which added an additional 25.4% of the variance (eigen-value of 1.27). For purposes of this investigation, it was decided to consider results for both the one and two factor solutions with the injury-related variables. Table 4 provides the intercorrelation of the medical variables as well as their loadings (correlations) on the derived factors.

TABLE 4 about here.

The factor from the first solution we termed GENALFAC. Those from the second were respectively termed MUSFAC and OTHRFACT. These terms were selected to reflect the relative prominence of general, muscular, and other symptom loadings on the respective factors (cf, Table 4).

The factor from the first solution with greatest loading was GENALFAC. This factor was selected to represent the general factor. The factor from the second solution with greatest loading was MUSFAC. This factor was selected to represent the muscular factor. The factor from the second solution with greatest loading was OTHRFACT. This factor was selected to represent the other factor.

Correlation of Medical and Injury-Related Variables

Stepwise regression analysis was applied to each of the three medical factor variables (i.e., GENFAC, MUSFAC and OTHRFACT). Interestingly, prior to the analyses, it had been planned to force specific variables (Maximum Shear, and absolute Axial Forces); however, these were selected from GENFAC and MUSFAC by the stepwise procedure. We also correlated G-level with these factor variables, but maximum shear or axial force showed a higher correlation. For OTHRFACT, the Shear and Axial Variables were unproductive and a broad range of other variables were considered (e.g. Torques at the condyles, etc.). Analyses for GENFAC and MUSFAC represent planned analyses while that for OTHRF was exploratory.

GENFAC.

Regression analysis with the shear and axial variables yielded a significant multiple $R = 0.354$ ($F(2,57) = 4.07$, $p < .025$). The prediction equation is:

$$\text{GENFAC} = -.7194 + .0027Z + .0028S \quad (1)$$

where Z is the greatest negative axial force (Newtons) and S is the maximum shear (Newtons). The coefficient for Z and S significantly exceeded their respective standard errors ($F(1,57) = 5.20$, $p < .05$ and $F(1,57) = 7.83$, $p < .01$). Equation (1) predicts an increasing GENFAC with increasing shear force and lessening of the axial force which tends to hold the head on the neck.



MUSFAC. Regression analysis with the axial and shear variables yielded a significant multiple $R^2 = 0.378$ ($F(2,57) = 4.75$, $p < .012$). The prediction equation is:

$$\text{MUSFAC} = -.8435 + .0025Z + .0029S \quad (2)$$
where Z and S are as defined for equation (1). Again the coefficient for Z and S significantly exceed their respective standard errors ($F(1,57) = 4.44$, $p < .05$ and $F(1,57) = 8.26$, $p < .01$). Equation (2) predicts increases in MUSFAC under conditions similar to that of (1).

OTHRFAC

Initial regression analysis with axial and shear forces yielded no results of consequence. Subsequent stepwise analysis was only relatively more productive; the best single predictor was the maximum torque about the X-axis ($R^2 = .18$, $p > .16$) which even in conjunction with a second predictor (greatest negative torque about the S-axis) yielded no improvement ($R^2 = 0.236$, $p > .19$). The resulting OTHRAC prediction equation weight for the torque variables were in the direction of increasing with increasing torque magnitude.

DISCUSSION

This report considered the relationship between variables believed to be injury-related and their correlation with medical findings over (-X), (+Y) and (-X+Y) impacts. Initial analyses focused upon relationships within the medical variables. These focused our attention on the relationship between the injury-related and medical factor variables. Our discussion of these results will follow this pattern of analysis and will precede conclusions.

Injury-Related Variables.

The graphical analyses of these variables revealed two relationships. First and not unexpectedly, the injury-related variables tended to increase with the nominal magnitudes for each vector direction exposure (cf, Figure 3, 4 and 5). This focused attention on the nominally most severe runs for each vector direction in the NBDL database.

The second finding of the graphical analyses was the apparent relationship between the injury-related criteria and anthropometry (i.e., head mass) seen in Figures 6, 7 and 8. Subject H132 with the largest head mass experienced larger forces and torques than the smallest (H135). These subjects also differed on other variables in a similar pattern (e.g. neck length) and consequently the observed systemic differences can not be uniquely ascribed to head mass. (However, the report by Muzzy et al. (3) certainly indicates a strong relationship between head mass and resultant forces and torques.) Interestingly subject H134, with an intermediate head mass reported no adverse effects and had a particularly short neck.



Currently, we are initiating correlation of variables across subjects in an effort to be more definitive. Certainly, these results point to consistent individual differences which are embedded in our later analyses.

Medical Findings

where \bar{X} and \bar{Y} are defined as the mean of the variables X and Y respectively. and Summary of the medical findings revealed apparent clusters of reported symptoms (cf, Table 3). These clusters could reflect subject tendencies to complain; subject differences in "injury"; or a combination of both. The tendency for subject H132 (largest head mass) to report more often than H135 (smallest) did give some initial support for the view that actual injury differences are involved. Factor analysis was performed to identify and condense the symptoms prior to correlation analyses with the injury-related variables. Table 4 standardized the correlation between the transformed medical variables and factors which resulted from this analysis.

Regression Analyses

The correlational analyses relating the medical factors and injury-related variables provided strong evidence of their relationship. Both the GENFAC (general) and the MUSFAC (muscle) factor variables exhibited moderate but highly significant ($p < .025$ and $.012$ respectively) correlation with the same shear and axial forces experienced by the subject ($r = .35$ and $.38$). The prediction equations for these two variables were also similar equation (cf, equations (1) and (2)). These similarities, were in part not unexpected as GENFAC may theoretically be viewed as a comparison between MUSFAC and OTHRAC. However, the correlation between MUSFAC and GENFAC was relatively higher than expected ($r = .86$). In any case, the relationship between the injury-related dynamic variables and the medical reports is supported by the results in the paper. The choice of symptom cluster does remain open for future work.

CONCLUSION

The findings of this report encourage continued systematic evaluation of the relationship between observed injury-related variables and medical findings. Certainly, the results of this report indicate a moderate but highly significant correlation between reported symptoms and the maximum shear and greatest negative axial forces. Based on this report, additional correlation analyses relating individual differences in anthropometric variables (head and neck size) with the injury-related and medical variables appears a fruitful direction for future work. Perhaps equally productive might be correlation of such variables and injuries experienced by civilian and military personnel in impact environments. We encourage other researchers to focus on non-permanent symptoms following impacts and their relationship with subject variables.



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[illegible]

Figure 1. The effect of the concentration of the *Agrobacterium* suspension on the transformation efficiency of *Agrobacterium* strains. The *Agrobacterium* strains were grown in the YEA medium for 24 h and then adjusted to the OD₆₀₀ of 0.1. The *Agrobacterium* strains were then grown in the YEA medium with the concentration of 0.1, 0.2, 0.3, 0.4, 0.5, 0.6, 0.7, 0.8, 0.9, 1.0, 1.1, 1.2, 1.3, 1.4, 1.5, 1.6, 1.7, 1.8, 1.9, 2.0, 2.1, 2.2, 2.3, 2.4, 2.5, 2.6, 2.7, 2.8, 2.9, 3.0, 3.1, 3.2, 3.3, 3.4, 3.5, 3.6, 3.7, 3.8, 3.9, 4.0, 4.1, 4.2, 4.3, 4.4, 4.5, 4.6, 4.7, 4.8, 4.9, 5.0, 5.1, 5.2, 5.3, 5.4, 5.5, 5.6, 5.7, 5.8, 5.9, 6.0, 6.1, 6.2, 6.3, 6.4, 6.5, 6.6, 6.7, 6.8, 6.9, 7.0, 7.1, 7.2, 7.3, 7.4, 7.5, 7.6, 7.7, 7.8, 7.9, 8.0, 8.1, 8.2, 8.3, 8.4, 8.5, 8.6, 8.7, 8.8, 8.9, 9.0, 9.1, 9.2, 9.3, 9.4, 9.5, 9.6, 9.7, 9.8, 9.9, 10.0, 10.1, 10.2, 10.3, 10.4, 10.5, 10.6, 10.7, 10.8, 10.9, 11.0, 11.1, 11.2, 11.3, 11.4, 11.5, 11.6, 11.7, 11.8, 11.9, 12.0, 12.1, 12.2, 12.3, 12.4, 12.5, 12.6, 12.7, 12.8, 12.9, 13.0, 13.1, 13.2, 13.3, 13.4, 13.5, 13.6, 13.7, 13.8, 13.9, 14.0, 14.1, 14.2, 14.3, 14.4, 14.5, 14.6, 14.7, 14.8, 14.9, 15.0, 15.1, 15.2, 15.3, 15.4, 15.5, 15.6, 15.7, 15.8, 15.9, 16.0, 16.1, 16.2, 16.3, 16.4, 16.5, 16.6, 16.7, 16.8, 16.9, 17.0, 17.1, 17.2, 17.3, 17.4, 17.5, 17.6, 17.7, 17.8, 17.9, 18.0, 18.1, 18.2, 18.3, 18.4, 18.5, 18.6, 18.7, 18.8, 18.9, 19.0, 19.1, 19.2, 19.3, 19.4, 19.5, 19.6, 19.7, 19.8, 19.9, 20.0, 20.1, 20.2, 20.3, 20.4, 20.5, 20.6, 20.7, 20.8, 20.9, 21.0, 21.1, 21.2, 21.3, 21.4, 21.5, 21.6, 21.7, 21.8, 21.9, 22.0, 22.1, 22.2, 22.3, 22.4, 22.5, 22.6, 22.7, 22.8, 22.9, 23.0, 23.1, 23.2, 23.3, 23.4, 23.5, 23.6, 23.7, 23.8, 23.9, 24.0, 24.1, 24.2, 24.3, 24.4, 24.5, 24.6, 24.7, 24.8, 24.9, 25.0, 25.1, 25.2, 25.3, 25.4, 25.5, 25.6, 25.7, 25.8, 25.9, 26.0, 26.1, 26.2, 26.3, 26.4, 26.5, 26.6, 26.7, 26.8, 26.9, 27.0, 27.1, 27.2, 27.3, 27.4, 27.5, 27.6, 27.7, 27.8, 27.9, 28.0, 28.1, 28.2, 28.3, 28.4, 28.5, 28.6, 28.7, 28.8, 28.9, 29.0, 29.1, 29.2, 29.3, 29.4, 29.5, 29.6, 29.7, 29.8, 29.9, 30.0, 30.1, 30.2, 30.3, 30.4, 30.5, 30.6, 30.7, 30.8, 30.9, 31.0, 31.1, 31.2, 31.3, 31.4, 31.5, 31.6, 31.7, 31.8, 31.9, 32.0, 32.1, 32.2, 32.3, 32.4, 32.5, 32.6, 32.7, 32.8, 32.9, 33.0, 33.1, 33.2, 33.3, 33.4, 33.5, 33.6, 33.7, 33.8, 33.9, 34.0, 34.1, 34.2, 34.3, 34.4, 34.5, 34.6, 34.7, 34.8, 34.9, 35.0, 35.1, 35.2, 35.3, 35.4, 35.5, 35.6, 35.7, 35.8, 35.9, 36.0, 36.1, 36.2, 36.3, 36.4, 36.5, 36.6, 36.7, 36.8, 36.9, 37.0, 37.1, 37.2, 37.3, 37.4, 37.5, 37.6, 37.7, 37.8, 37.9, 38.0, 38.1, 38.2, 38.3, 38.4, 38.5, 38.6, 38.7, 38.8, 38.9, 39.0, 39.1, 39.2, 39.3, 39.4, 39.5, 39.6, 39.7, 39.8, 39.9, 40.0, 40.1, 40.2, 40.3, 40.4, 40.5, 40.6, 40.7, 40.8, 40.9, 41.0, 41.1, 41.2, 41.3, 41.4, 41.5, 41.6, 41.7, 41.8, 41.9, 42.0, 42.1, 42.2, 42.3, 42.4, 42.5, 42.6, 42.7, 42.8, 42.9, 43.0, 43.1, 43.2, 43.3, 43.4, 43.5, 43.6, 43.7, 43.8, 43.9, 44.0, 44.1, 44.2, 44.3, 44.4, 44.5, 44.6, 44.7, 44.8, 44.9, 45.0, 45.1, 45.2, 45.3, 45.4, 45.5, 45.6, 45.7, 45.8, 45.9, 46.0, 46.1, 46.2, 46.3, 46.4, 46.5, 46.6, 46.7, 46.8, 46.9, 47.0, 47.1, 47.2, 47.3, 47.4, 47.5, 47.6, 47.7, 47.8, 47.9, 48.0, 48.1, 48.2, 48.3, 48.4, 48.5, 48.6, 48.7, 48.8, 48.9, 49.0, 49.1, 49.2, 49.3, 49.4, 49.5, 49.6, 49.7, 49.8, 49.9, 50.0, 50.1, 50.2, 50.3, 50.4, 50.5, 50.6, 50.7, 50.8, 50.9, 51.0, 51.1, 51.2, 51.3, 51.4, 51.5, 51.6, 51.7, 51.8, 51.9, 52.0, 52.1, 52.2, 52.3, 52.4, 52.5, 52.6, 52.7, 52.8, 52.9, 53.0, 53.1, 53.2, 53.3, 53.4, 53.5, 53.6, 53.7, 53.8, 53.9, 54.0, 54.1, 54.2, 54.3, 54.4, 54.5, 54.6, 54.7, 54.8, 54.9, 55.0, 55.1, 55.2, 55.3, 55.4, 55.5, 55.6, 55.7, 55.8, 55.9, 56.0, 56.1, 56.2, 56.3, 56.4, 56.5, 56.6, 56.7, 56.8, 56.9, 57.0, 57.1, 57.2, 57.3, 57.4, 57.5, 57.6, 57.7, 57.8, 57.9, 58.0, 58.1, 58.2, 58.3, 58.4, 58.5, 58.6, 58.7, 58.8, 58.9, 59.0, 59.1, 59.2, 59.3, 59.4, 59.5, 59.6, 59.7, 59.8, 59.9, 60.0, 60.1, 60.2, 60.3, 60.4, 60.5, 60.6, 60.7, 60.8, 60.9, 61.0, 61.1, 61.2, 61.3, 61.4, 61.5, 61.6, 61.7, 61.8, 61.9, 62.0, 62.1, 62.2, 62.3, 62.4, 62.5, 62.6, 62.7, 62.8, 62.9, 63.0, 63.1, 63.2, 63.3, 63.4, 63.5, 63.6, 63.7, 63.8, 63.9, 64.0, 64.1, 64.2, 64.3, 64.4, 64.5, 64.6, 64.7, 64.8, 64.9, 65.0, 65.1, 65.2, 65.3, 65.4, 65.5, 65.6, 65.7, 65.8, 65.9, 66.0, 66.1, 66.2, 66.3, 66.4, 66.5, 66.6, 66.7, 66.8, 66.9, 67.0, 67.1, 67.2, 67.3, 67.4, 67.5, 67.6, 67.7, 67.8, 67.9, 68.0, 68.1

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On 11 February 1968, the following information was received from the American Consulate in London:



Table 1. Subject Anthropometric Variables

| Subject | Age (Yrs) | Height (cm) | Weight (kg) | Head Circumference (cm) | Head Length (cm) |
|---------|--------------|----------------|----------------|-------------------------------|------------------------|
| H131 | 20 | 167.0 | 67.7 | 57.5 | 19.6 |
| H132 | 21 | 172.9 | 80.0 | 57.9 | 19.7 |
| H133 | 20 | 161.7 | 61.4 | 56.1 | 19.4 |
| H134 | 20 | 178.3 | 75.5 | 56.6 | 19.4 |
| H135 | 23 | 171.6 | 69.1 | 53.5 | 17.9 |
| H136 | 19 | 185.4 | 89.1 | 56.4 | 19.4 |

Table 2. HEAD MASS PARAMETERS

| SUBJECT | MASS* (gm) | CENTER OF MASS** (cm) | | | PRINCIPAL MOMENTS** OF INERTIAL (Kg-cm(2)) | | |
|---------|---------------|--------------------------|------|------|---|-------|-------|
| | | X | Y | Z | X' | Y' | Z' |
| H131 | 4449 | 0.84 | -.06 | 3.17 | 219.8 | 235.0 | 152.9 |
| H132 | 4523 | 0.84 | -.06 | 3.18 | 225.9 | 241.5 | 157.2 |
| H133 | 4170 | 0.82 | -.05 | 3.10 | 197.3 | 211.0 | 137.3 |
| H134 | 4278 | 0.83 | -.05 | 3.13 | 205.9 | 220.1 | 143.3 |
| H135 | 3791 | 0.80 | -.05 | 3.00 | 168.3 | 180.0 | 117.1 |
| H136 | 4235 | 0.83 | -.05 | 3.12 | 202.4 | 216.4 | 140.9 |

*Mass estimated from head circumference and length (Kaleps et al., 1984)

**Center of mass and principal moments estimated via isometric analysis (Bittner, 1986)



| RUN NUMBER | SUBJECT NUMBER | G level | MUSCLE SORENESS (HOURS) | MUSCLE STIFFNESS (HOURS) | HEADACHE (HOURS) | BACKACHE (HOURS) | OTHE (YES/N |
|---------------|-------------------|-------------|-------------------------------|--------------------------------|---------------------|---------------------|----------------|
| 3908 | H131 | 10.2G(-x) | | | | | |
| 3948 | H131 | 13.7G(-x) | | | | | |
| 3987 | H131 | 14.5G(-x) | | | | | |
| 3990 | H131 | 15.4G(-x) | | | | | |
| 4089 | H131 | 5.1G(+y) | | | | | |
| 4109 | H131 | 6.2G(+y) | | | | | |
| 4124 | H131 | 7.2G(+y) | | | | | |
| 4242 | H131 | 7.3G(-x+y) | | | | | YES* |
| 4251 | H131 | 10.2G(-x+y) | | | | | YES |
| 3989 | H132 | 10.3G(-x) | 59 | 59 | | | |
| 3950 | H132 | 13.6G(-x) | 68 | 68 | | | |
| 3957 | H132 | 14.7G(-x) | 33 | 33 | 7 | | |
| 3982 | H132 | 15.6G(-x) | 49 | 49 | 4 | | |
| 4090 | H132 | 5.1G(+y) | 67 | 67 | | | |
| 4110 | H132 | 6.1G(+y) | 70 | 70 | | 67 | |
| 4128 | H132 | 7.1G(+y) | 47 | | | | |
| 4261 | H132 | 9.0G(-x+y) | | | | | |
| 4297 | H132 | 10.0G(-x+y) | | | | | |
| 4306 | H132 | 11.1G(-x+y) | 48 | | 33 | 48 | YES* |
| 3998 | H133 | 10.2G(-x) | | | | | |
| 3951 | H133 | 13.4G(-x) | | | | | |
| 3963 | H133 | 14.5G(-x) | | | | | |
| 3986 | H133 | 15.6G(-x) | | | | | |
| 4093 | H133 | 5.1G(+y) | | | | | |
| 4111 | H133 | 6.1G(+y) | | | | | |
| 4125 | H133 | 7.2G(+y) | | | | | |
| 4236 | H133 | 7.3G(-x+y) | 44 | 44 | 6 | | |
| 4240 | H133 | 9.1G(-x+y) | 95 | 95 | 2 | | |
| | | | | | 11 | | |
| 3993 | H134 | 10.2G(-x) | | | | | |
| 3961 | H134 | 13.4G(-x) | | | | | |
| 3968 | H134 | 14.3G(-x) | | | | | |
| 3983 | H134 | 15.6G(-x) | | | | | |
| 4097 | H134 | 5.0G(+y) | | | | | |
| 4112 | H134 | 6.1G(+y) | | | | | |
| 4126 | H134 | 7.1G(+y) | | | | | |
| 4264 | H134 | 9.3G(-x+y) | | | | | |
| 4298 | H134 | 10.1G(-x+y) | | | | | |
| 4307 | H134 | 11.4G(-x+y) | | | | | |

* two premature ventricular contractions after impact.
 ** right bundle branch block for three complexes impact
 *** felt "stunned" after impact, complained of dizziness for 2 days



| RUN NUMBER | SUBJECT NUMBER | G level | MUSCULE SORENESS (HOURS) | MUSCLE STIFFNESS (HOURS) | HEADACHE (HOURS) | BACKACHE (HOURS) | OTHE (YES/N |
|---------------|-------------------|-------------|--------------------------------|--------------------------------|---------------------|---------------------|----------------|
| 3916 | H135 | 10.3G(-x) | | | | | |
| 3955 | H135 | 13.6G(-x) | | 18 | | | |
| 3965 | H135 | 14.6G(-x) | | | | | |
| 3970 | H135 | 15.6G(-x) | | | | | |
| 4095 | H135 | 5.2G(+y) | | | | | |
| 4114 | H135 | 6.1G(+y) | | | | | |
| 4131 | H135 | 7.3G(+y) | 44 | 44 | | | |
| 4314 | H135 | 9.1G(-x+y) | | | | | |
| 4316 | H135 | 10.1G(-x+y) | | | | | |
| | | 10.2G(-x) | | | | | |
| 4918 | H136 | 10.2G(-x) | | 20 | | | |
| 3953 | H136 | 13.3G(-x) | 33 | 33 | | | |
| 3962 | H136 | 14.1G(-x) | 47 | 47 | | | |
| 4098 | H136 | 5.1G(+) | | | 47 | 47 | |
| 4142 | H136 | 6.0G(+y) | | | | | YES |
| 4153 | H136 | 7.1G(+y) | | | | | |
| 4247 | H136 | 7.1G(-x+y) | | | | | |
| 4263 | H136 | 9.2G(-x+y) | 240 | | | | |

**** one premature ventricular contraction 22 seconds after impact



TABLE 4. MEDICAL VARIABLE INTERCORRELATIONS AND FACTOR LOADINGS

| MEDICAL VARIABLES | | | | | ONE FACTOR SOLUTION FACTOR | TWO FACTOR SOLUTION | |
|-------------------|-------|-------|-------|-------|----------------------------------|------------------------|-----------------------|
| MUSOR | MUSIF | HEAD | BACK | OTHER | (GENFAC) | FACTOR 1 (MUSFAC) | FACTOR 2 (OTHRFAC) |
| MUSOR | 1.000 | | | | | | |
| MUSIF | .800 | 1.000 | | | .856 | .901 | .169 |
| HEAD | .498 | .412 | 1.000 | | .775 | .929 | -.032 |
| BACK | .402 | .286 | .588 | 1.000 | .797 | .549 | .629 |
| OTHER | .046 | -.114 | .250 | .289 | 1.000 | .717 | .715 |
| | | | | | .232 | -.232 | .823 |

Pressure ventricular contraction 22 seconds after arrival



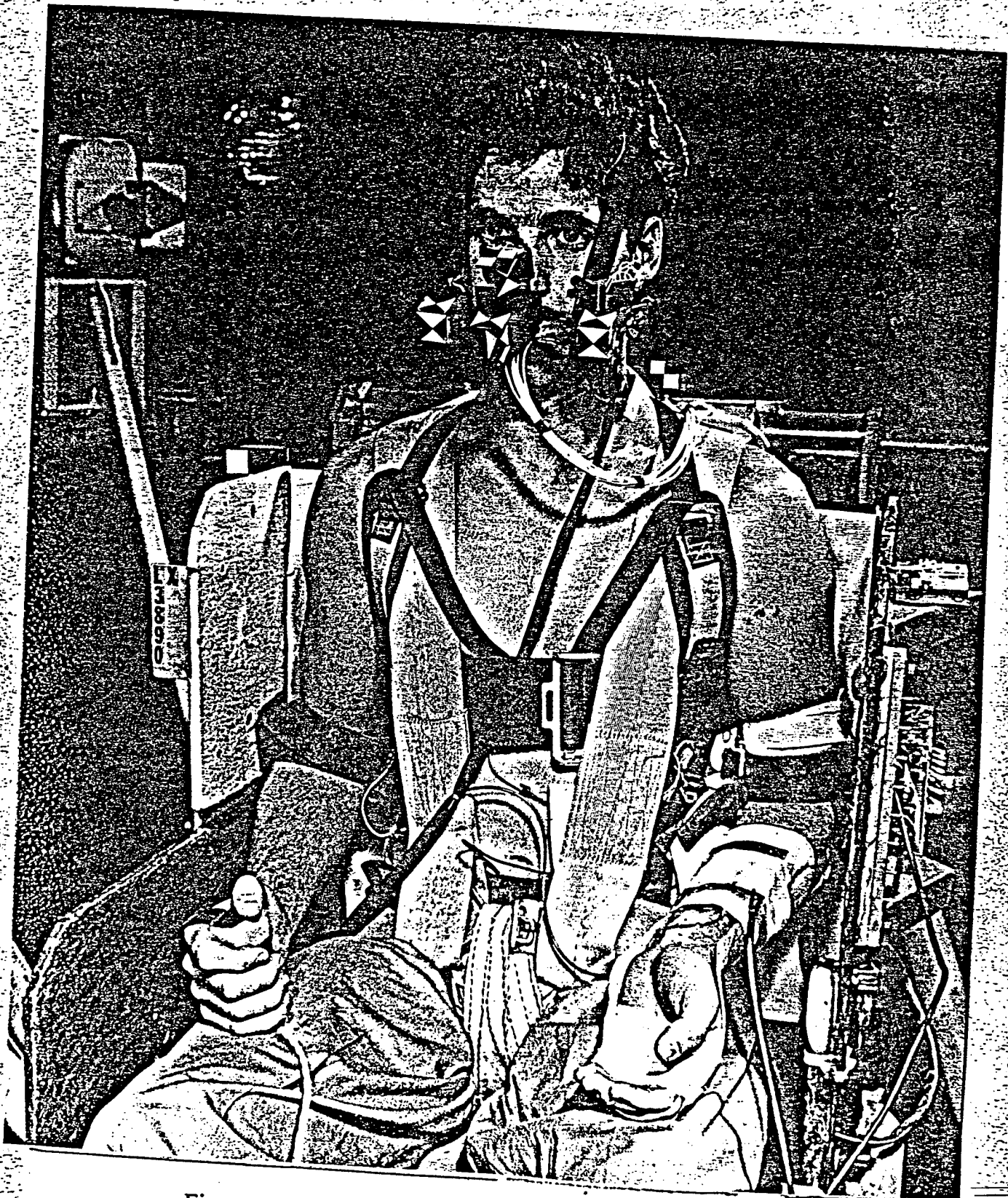
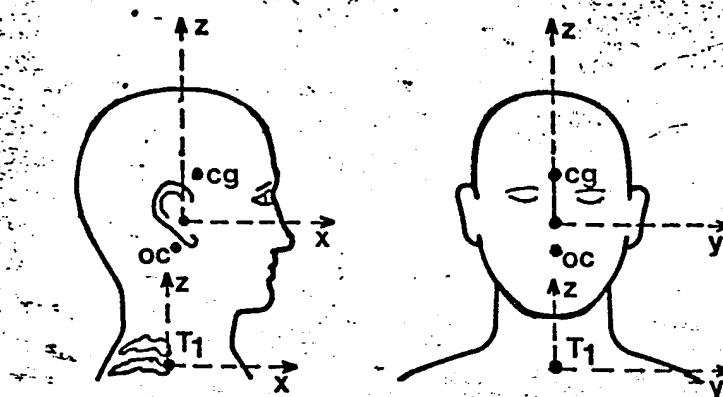


Figure 1, Illustration of the Restraint System as implemented on Subject H134.





**FIGURE 2. HEAD AND T1 ANATOMICAL
COORDINATE SYSTEMS**



Figure 3. Resultant Force Time-Courses Across -X, +Y, And -X+Y
Vector Directions And Selected Accelerations For H134

COORDINATE



RESULTANT FORCE FOR MINUS X SLED RUNS

| LEGEND | |
|-----------------|---------------|
| LX3993 R.J.FORE | H00134 10.70 |
| LX3991 R.J.FORE | H00134 13.40G |
| LX3998 R.J.FORE | H00134 14.31G |
| LX3983 R.J.FORE | H00134 15.58G |

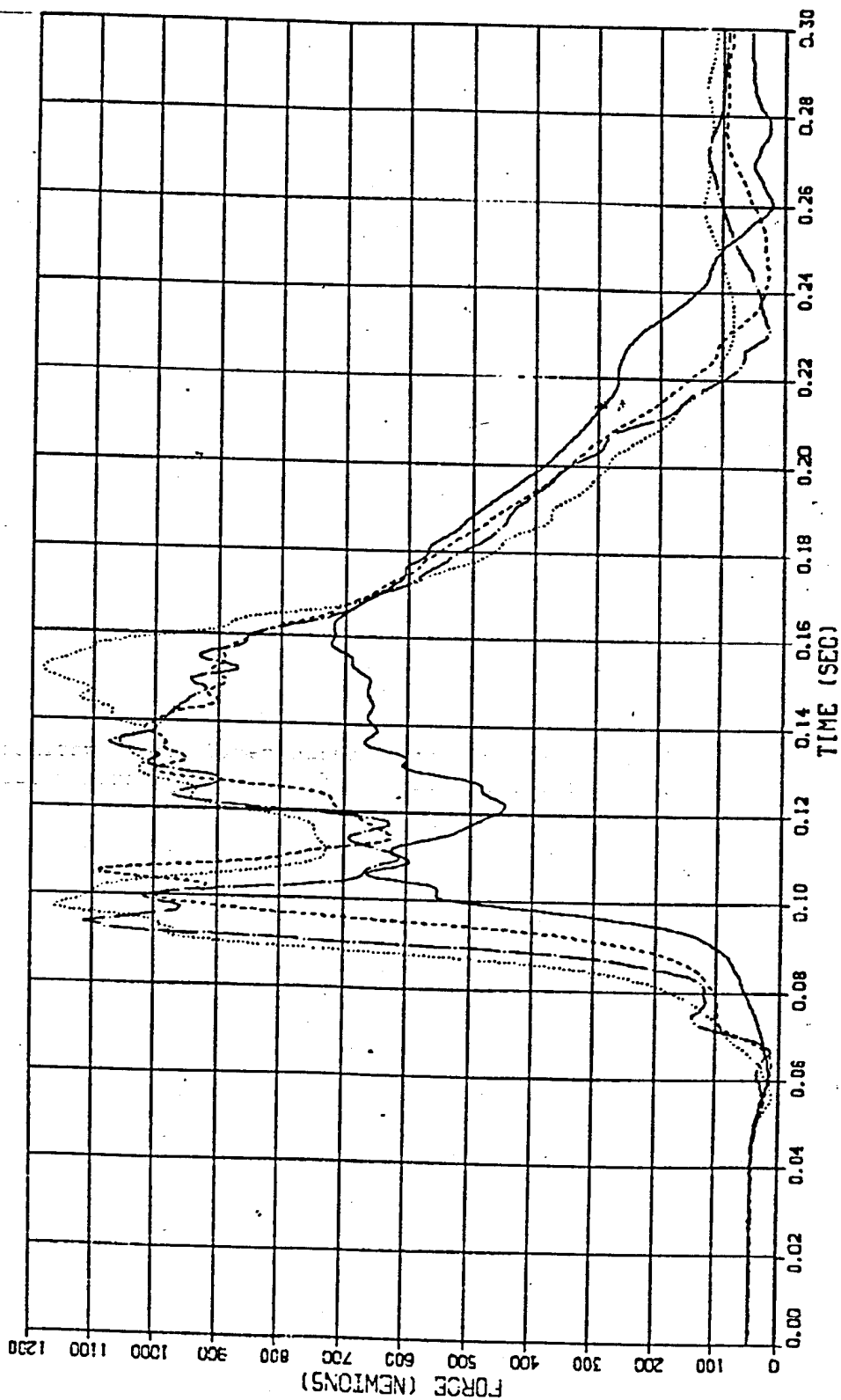


Fig 39

RESULTANT FORCE FOR PLUS Y SLED RUNS

| LEGEND | |
|---------------|--------------|
| LX4097 RJFORE | H00134 5.02G |
| LX4112 RJFORE | H00134 6.11G |
| LX4126 RJFORE | H00134 7.08G |

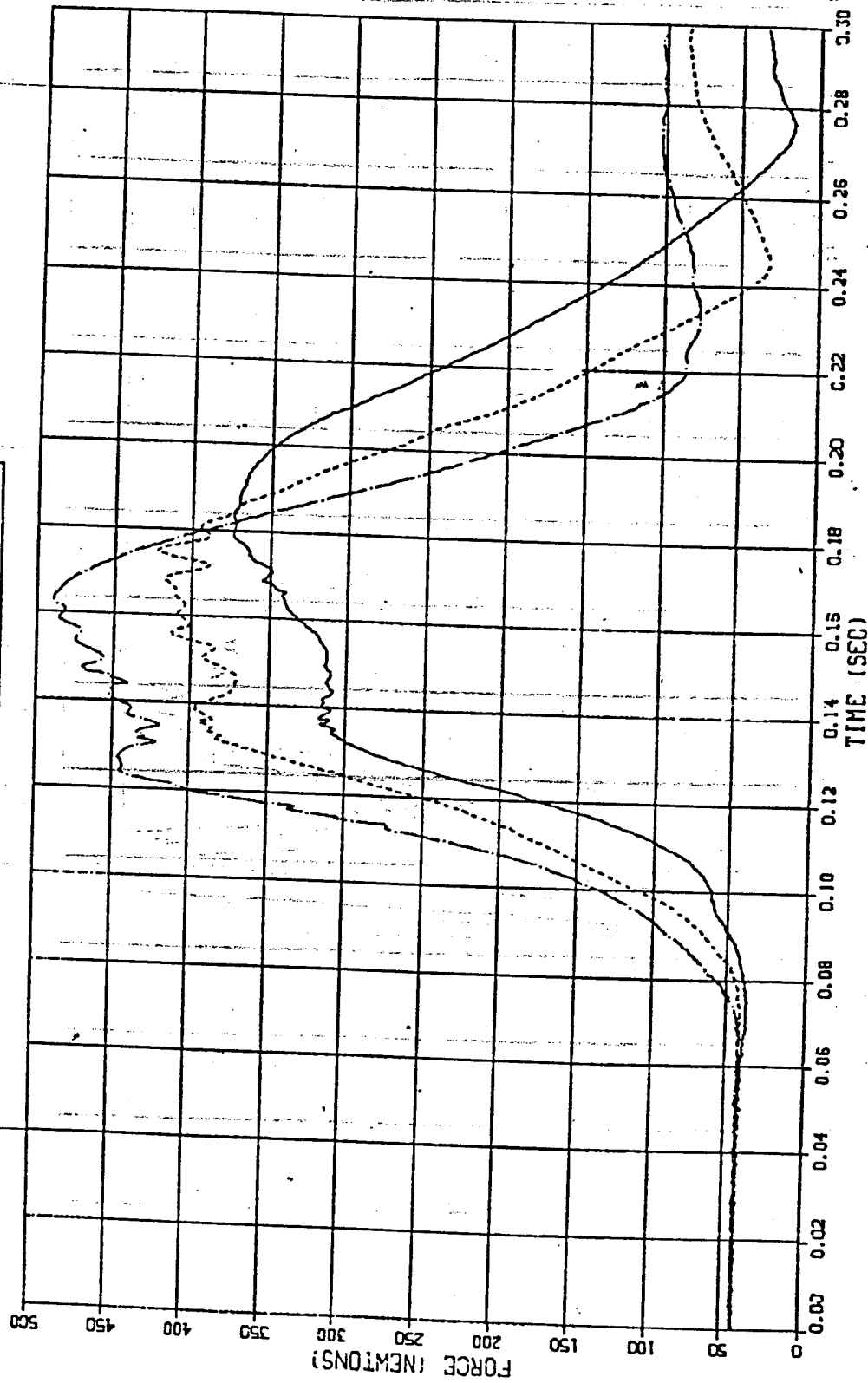


Fig 36

RESULTANT FORCE FOR MINUS X : PLUS Y SLED RUNS

| LEGEND | |
|----------------|---------------|
| LX1264 R-JFORE | H00134 0.270 |
| LX1298 R-JFORE | H00134 10.150 |
| LX1307 R-JFORE | H00134 11.440 |

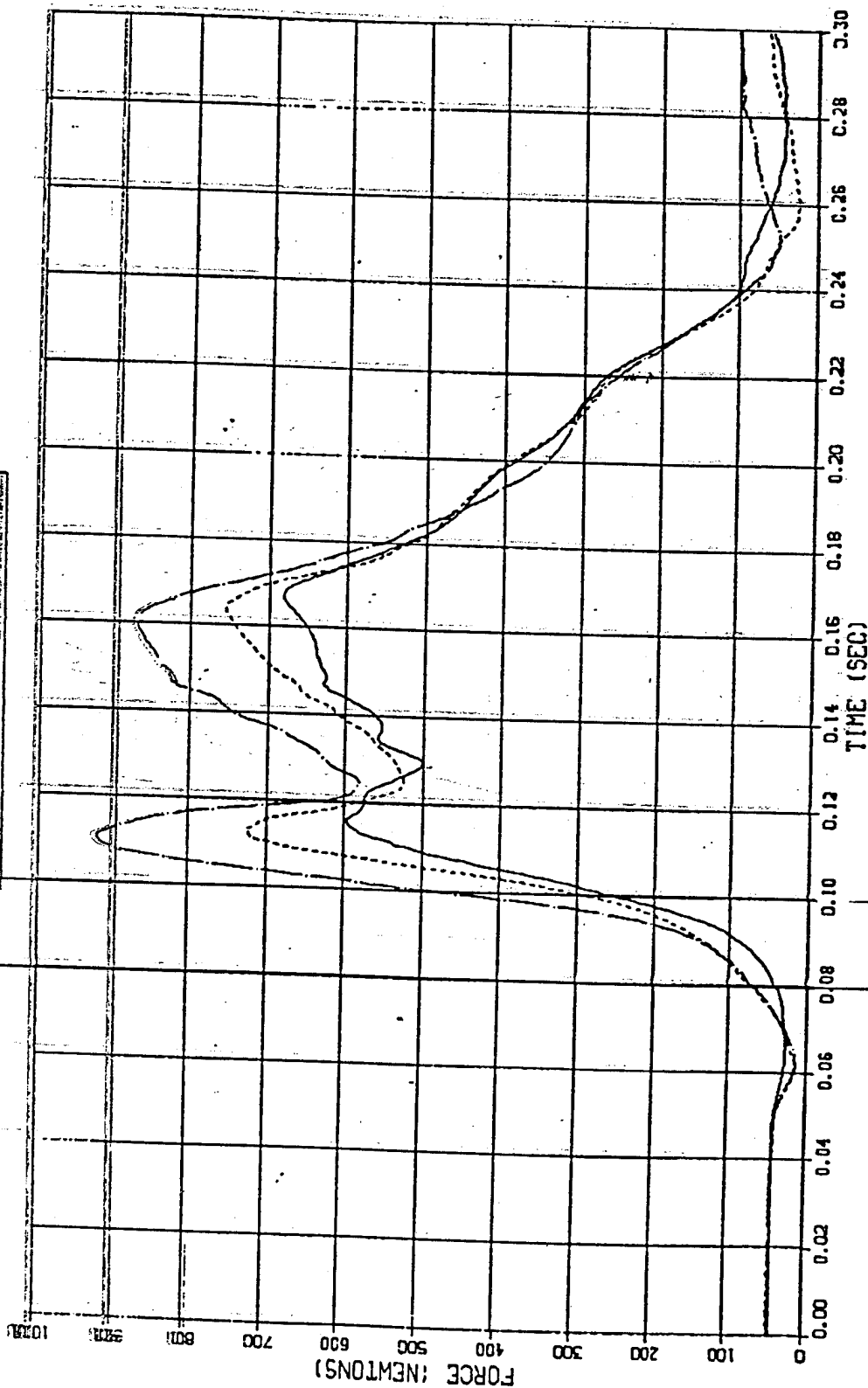


Fig 3c



Figure 4. Resultant Torque Time-Courses Across $-X$, $+Y$ and $-X+Y$
Vector Directions and Selected Accelerations For H134



RESULTANT TORQUE FOR MINUS X SLED RUNS

| LEGEND | |
|---------------|---------------|
| LX3963 RJTORO | H00134 10.178 |
| LX3961 RJTORO | H00134 13.406 |
| LX3968 RJTORO | H00134 14.316 |
| LX3983 RJTORO | H00134 15.586 |

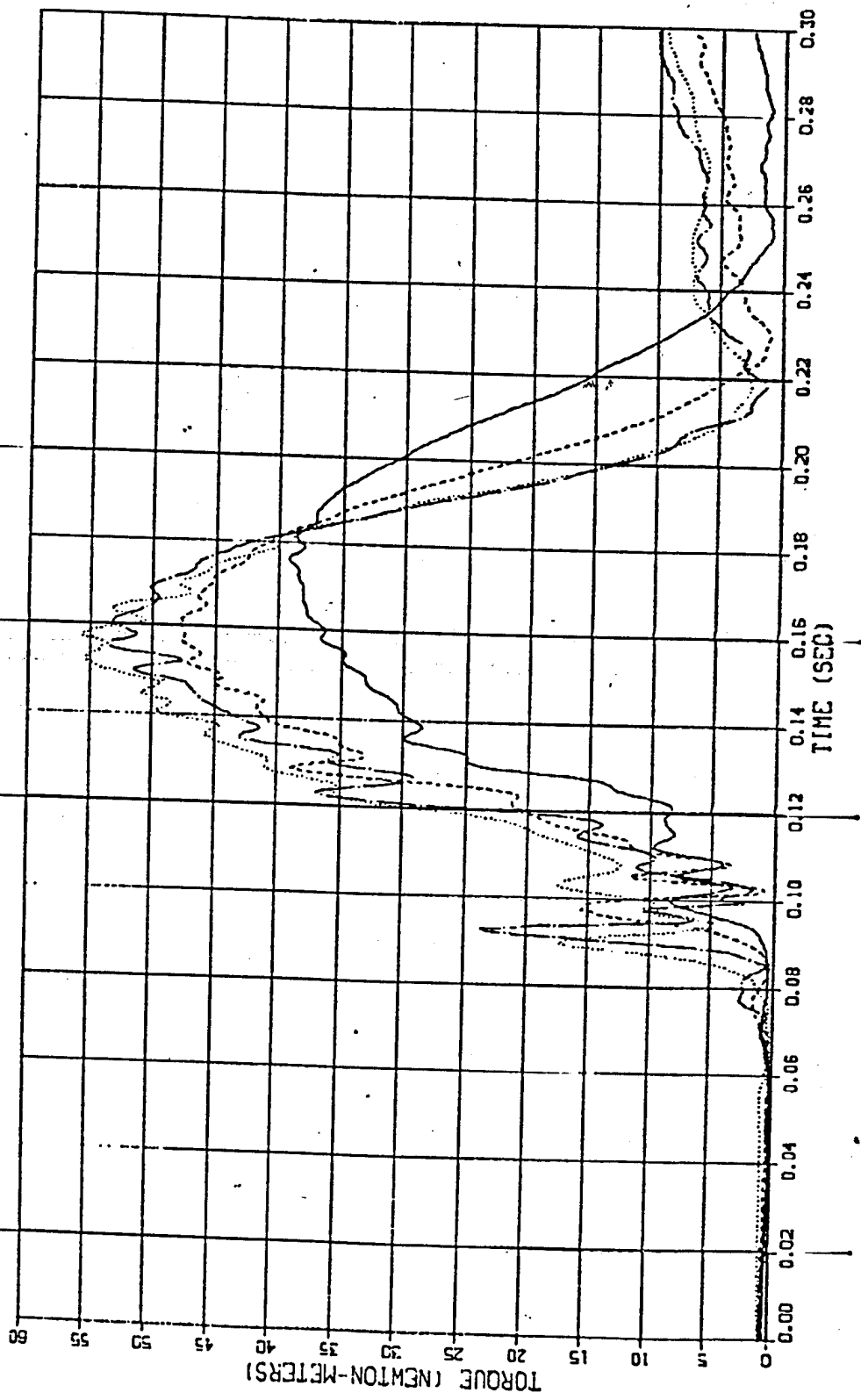


Fig 49



RESULTANT TORQUE FOR PLUS Y SLED RUNS

| LEGEND: | | |
|---------|--------|--------------|
| LX4097 | RJTORQ | H00134 5.02G |
| LX4112 | RJTORQ | H00134 6.11G |
| LX4126 | RJTORQ | H00134 7.08G |

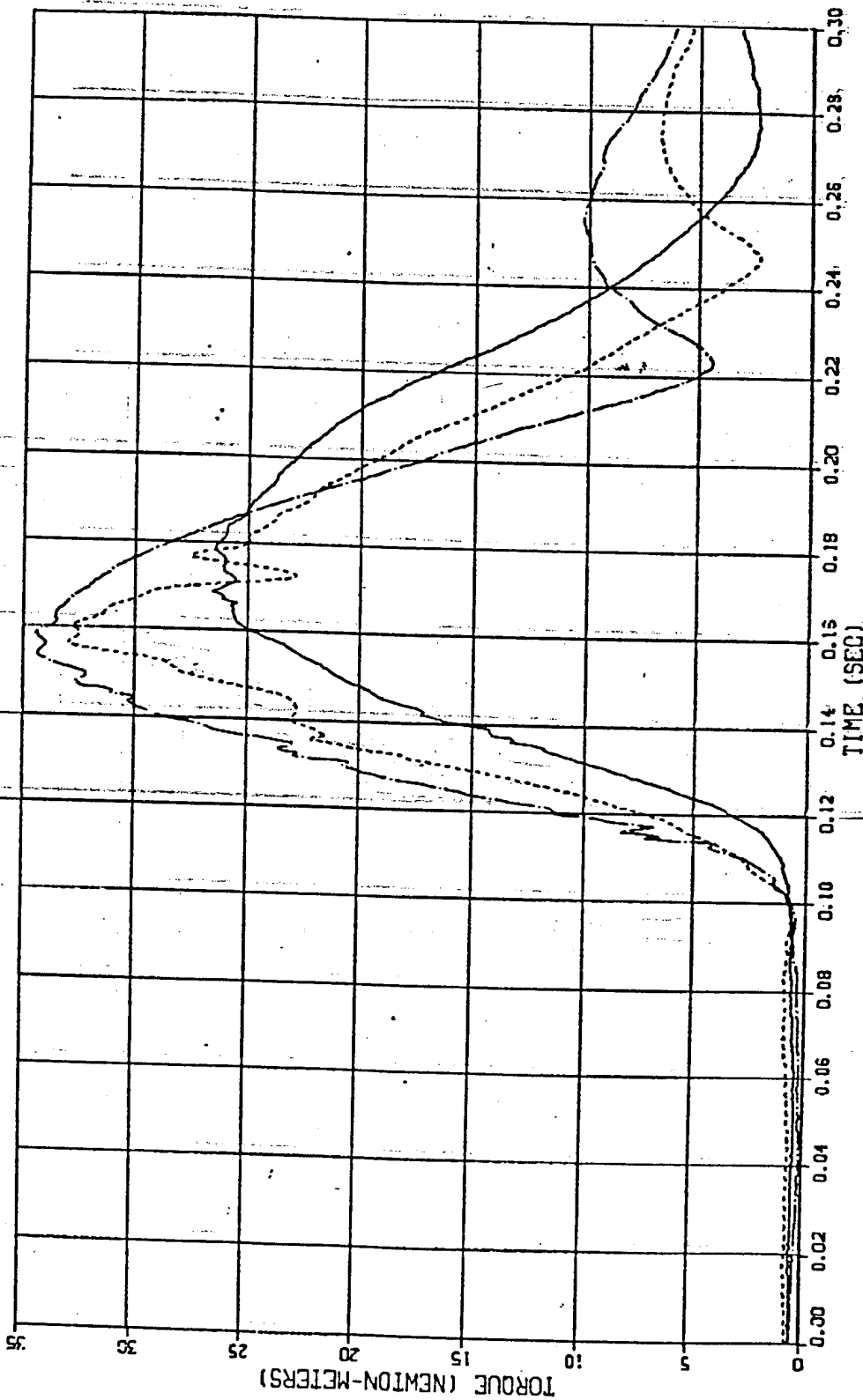


Fig 46



RESULTANT TORQUE FOR MINUS X : PLUS Y SLED RUNS

| LEGEND | |
|---------------|---------------|
| LX4264 RJTORQ | ADD134 0.276 |
| LX4298 RJTORQ | ADD134 10.136 |
| LX4307 RJTORQ | ADD134 11.446 |

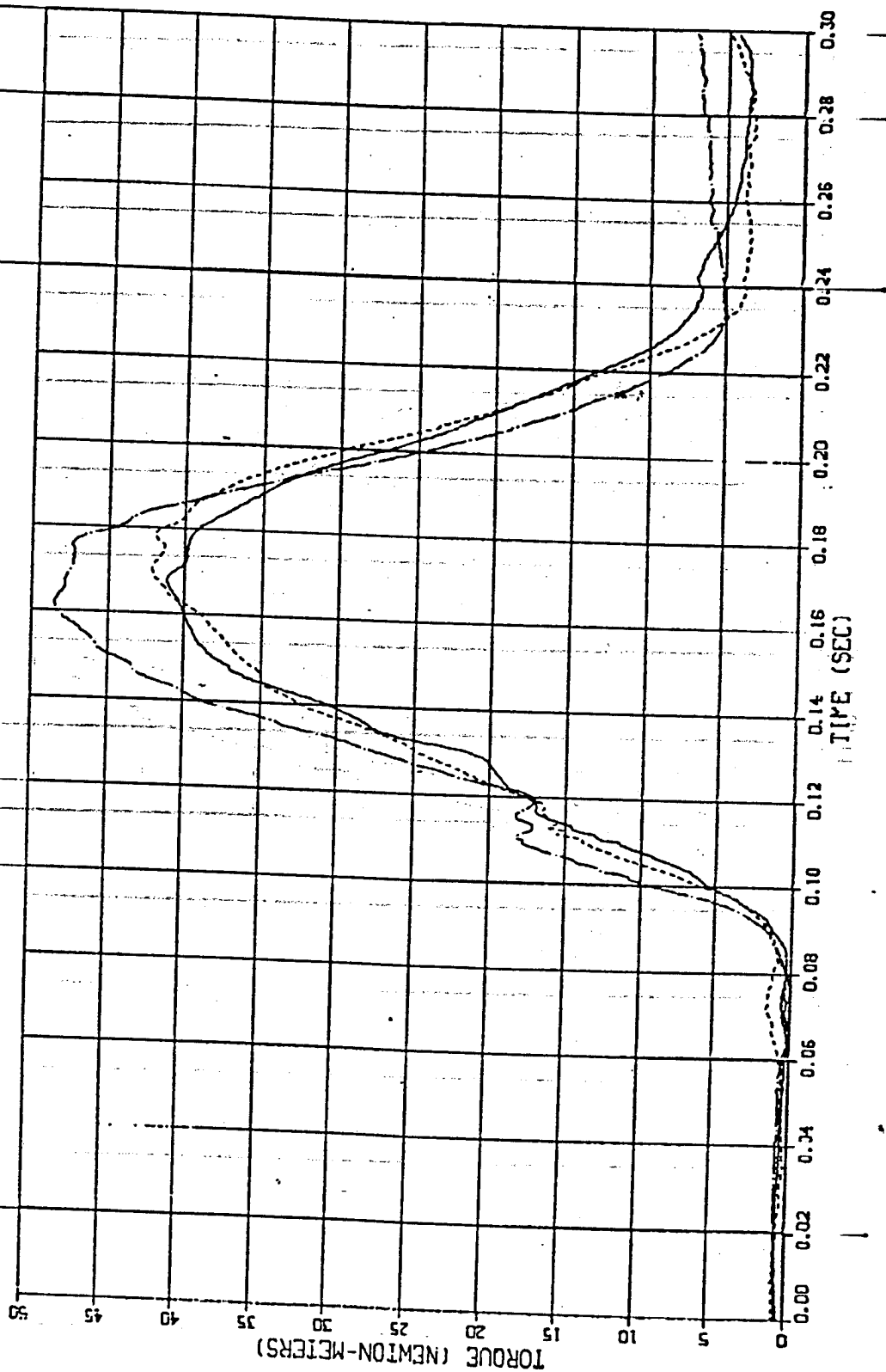


Fig 4C



Figure 5. Head Injury Criteria (HIC) Time-Courses Across -X, +Y and -X+Y
Vector Directions and Selected Accelerations For H134.



HEAD INJURY CRITERIA FOR MINUS X SLED RUNS

| LEGEND | |
|---------------|---------------|
| LX3993 HICAAA | H00134 10.17G |
| LX3961 HICAAA | H00134 13.40G |
| LX3968 HICAAA | H00134 14.31G |
| LX3983 HICAAA | H00134 15.58G |

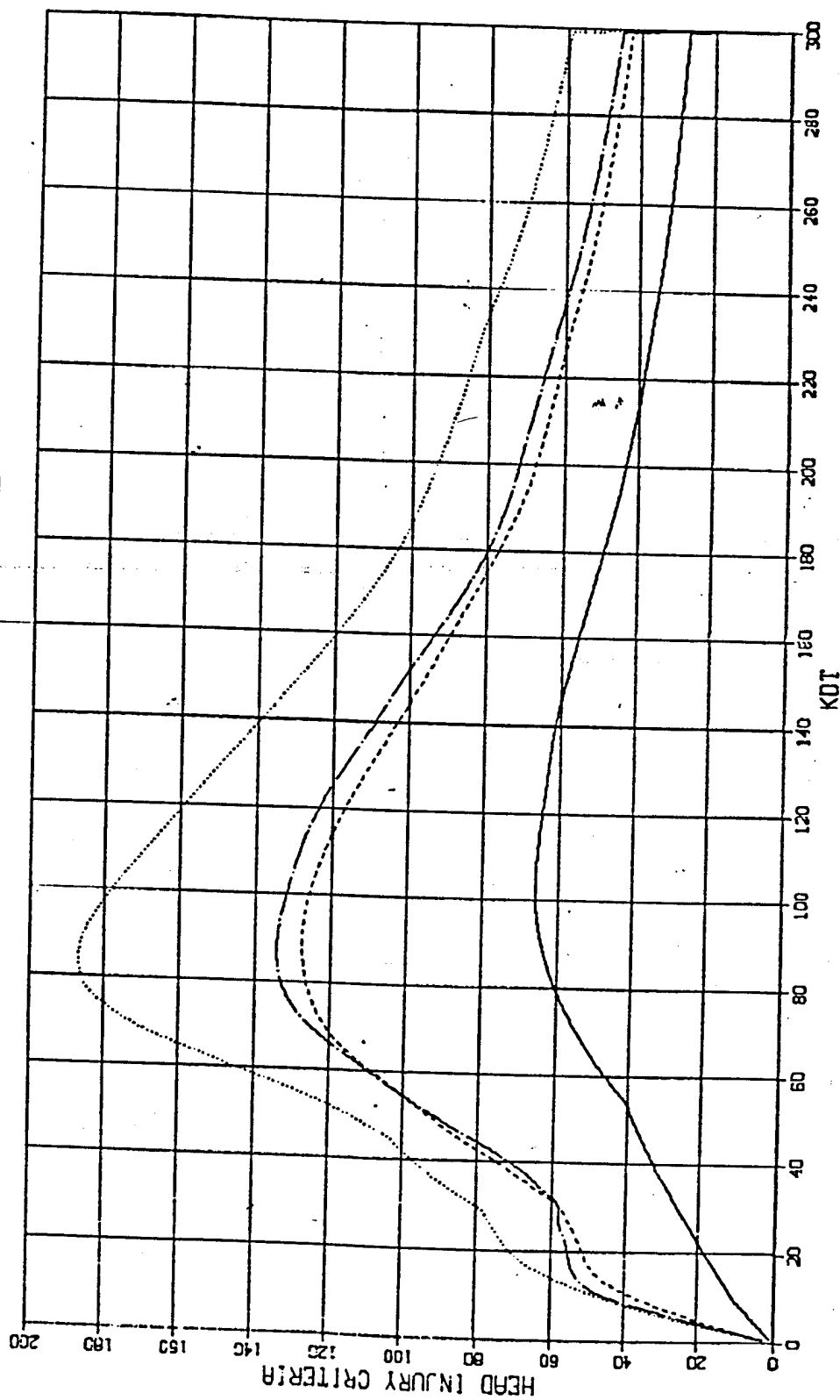


Fig 59



HEAD INJURY CRITERIA FOR PLUS Y SLED RUNS

| LEGEND | | |
|---------------|--------|-------|
| LX4097-HICAAA | H00134 | 5.02G |
| LX4112-HICAAA | H00134 | 5.11G |
| LX4126-HICAAA | H00134 | 7.08G |

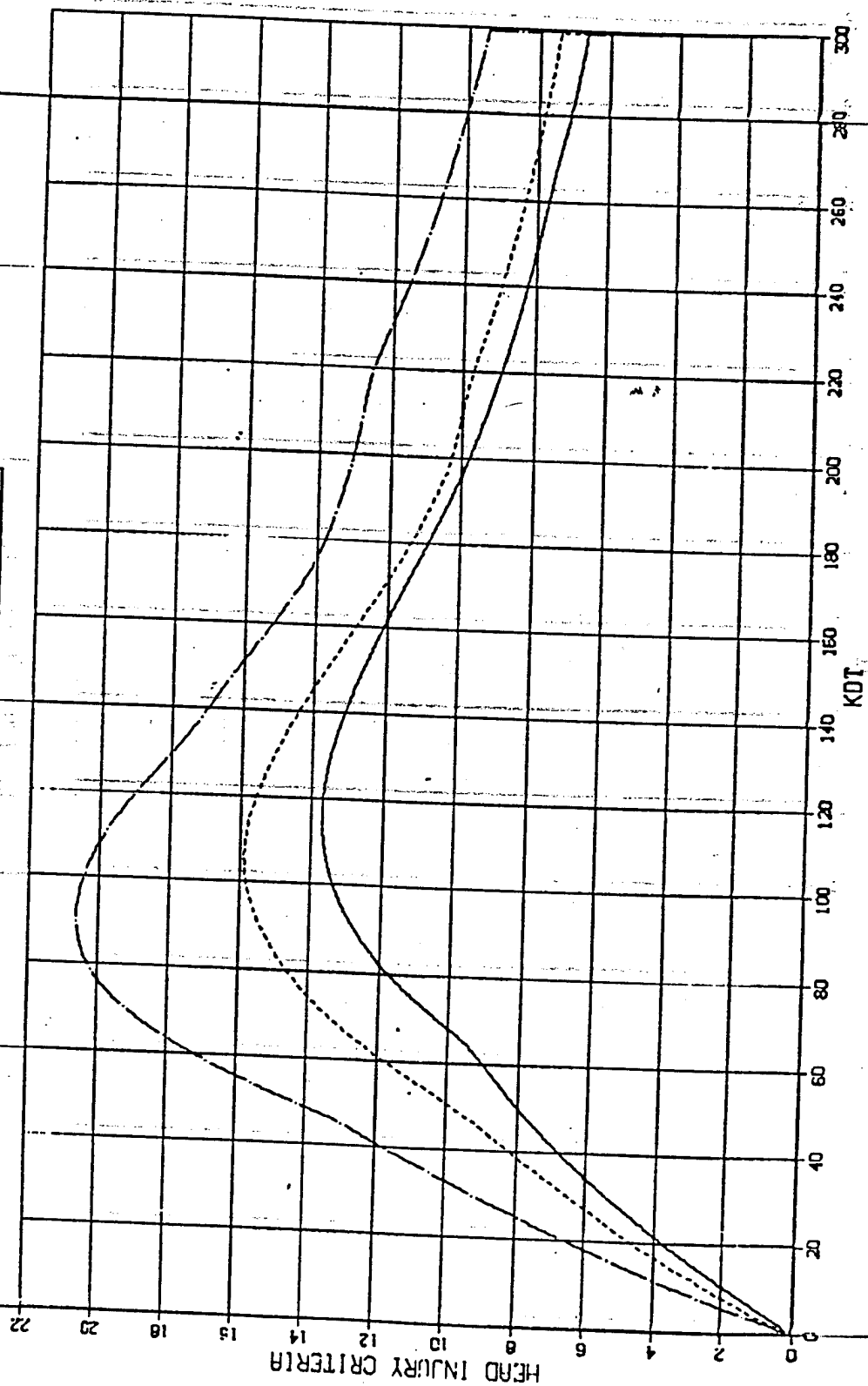


Fig 5b



HEAD INJURY CRITERIA FOR MINUS X 1 PLUS Y SLED RUNS

LEGEND

LX4264 HIC₁₅ 9.270
 LX4289 HIC₁₅ 10.136
 LX4307 HIC₁₅ 11.446

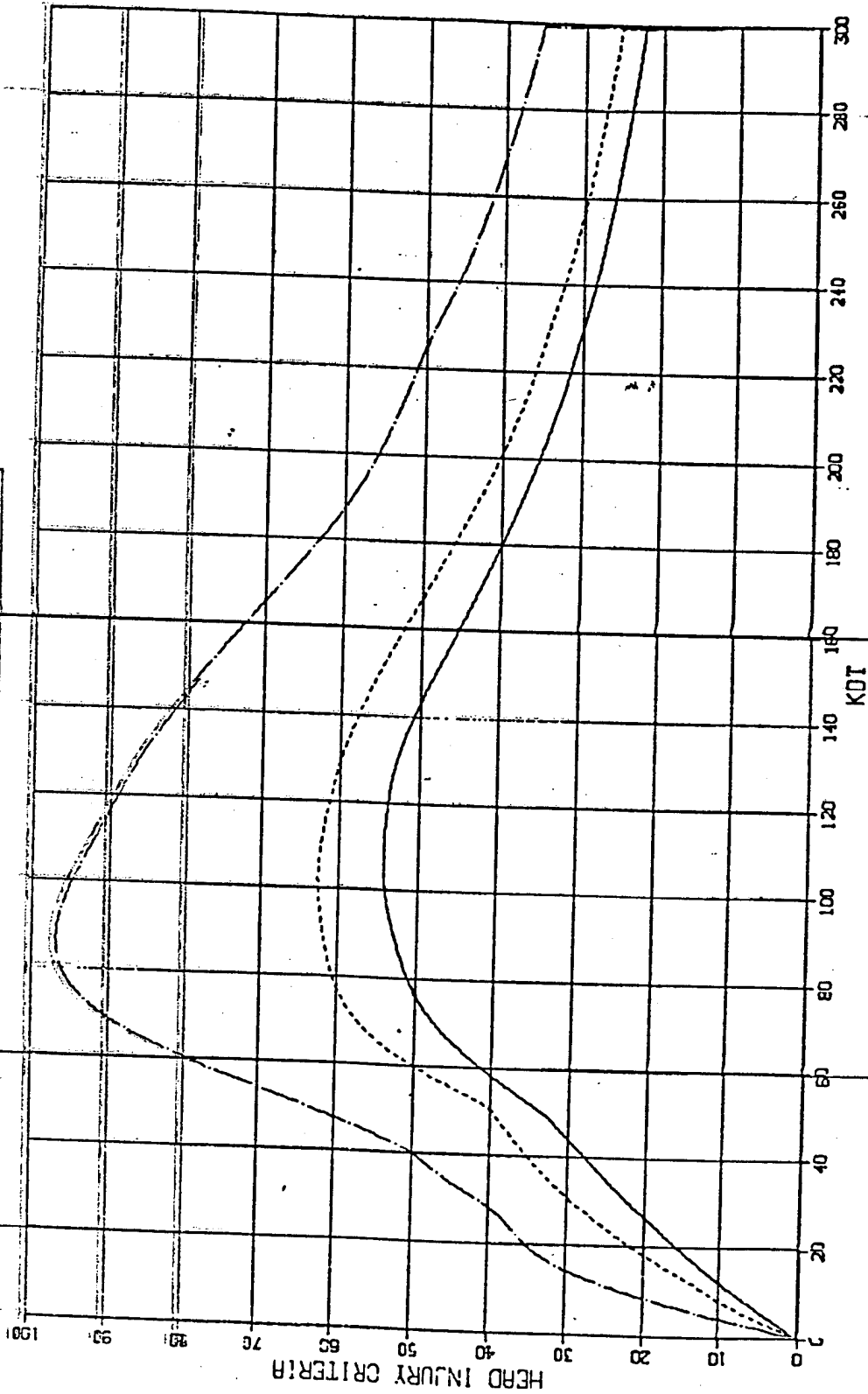


Fig 5C



Figure 6. Shear Force Time-Course Comparisons for Subjects with Large (H132) and Small (H135) Heads Across Selected -X, +Y, and -X+Y Impacts





SHEAR FORCE FOR MINUS X SLED DIRECTION

LEGEND

LX3982 SHFOREX H00132 15.61G
LX3970 SHFOREX H00135 15.55G

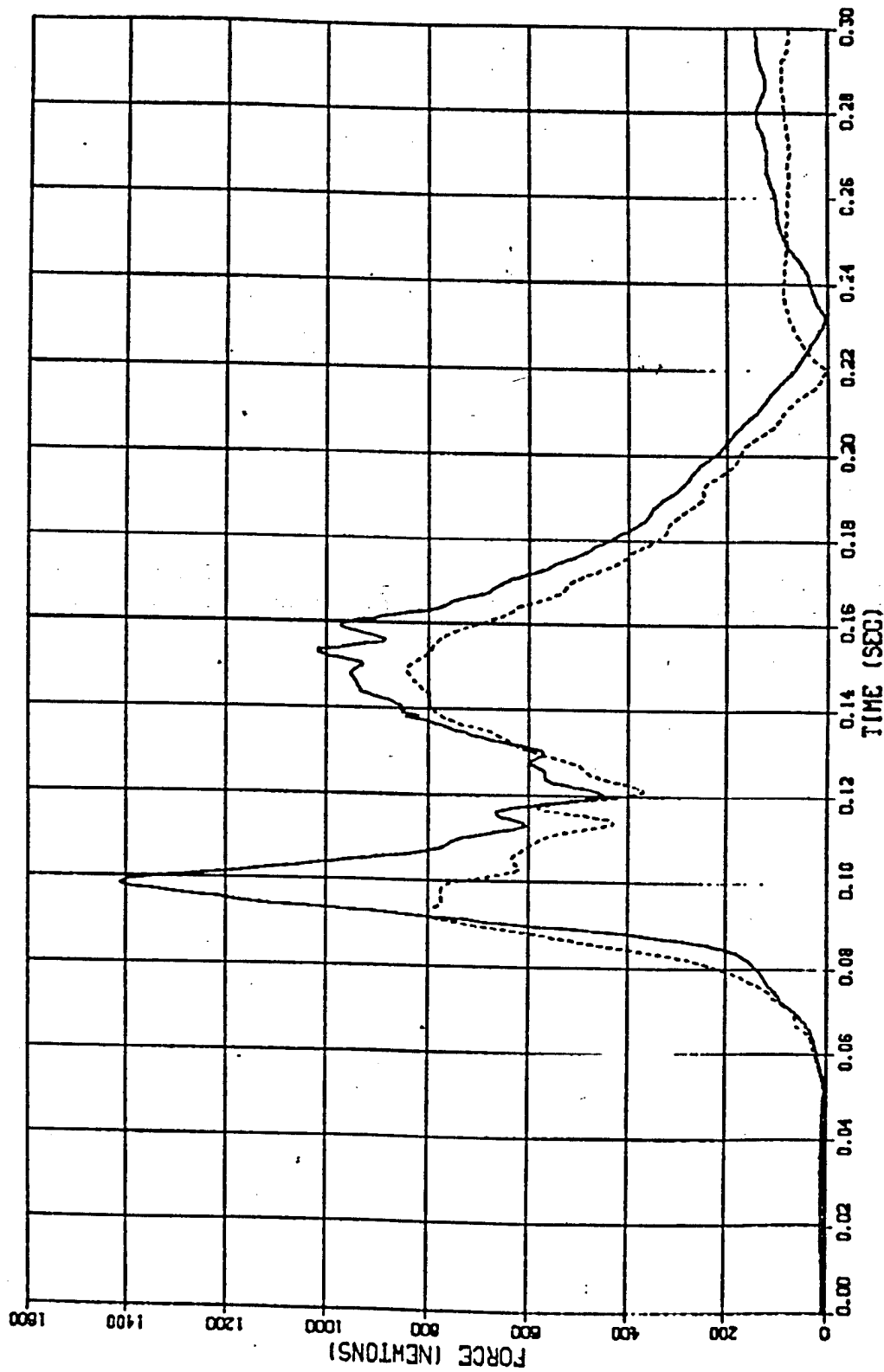


Fig 69



SHEAR FORCE FOR MINUS X : PLUS Y SLED RUNS

LEGEND
 LX4297 SHFOREX H00132 10.03G
 LX4316 SHFOREX H00135 10.07G

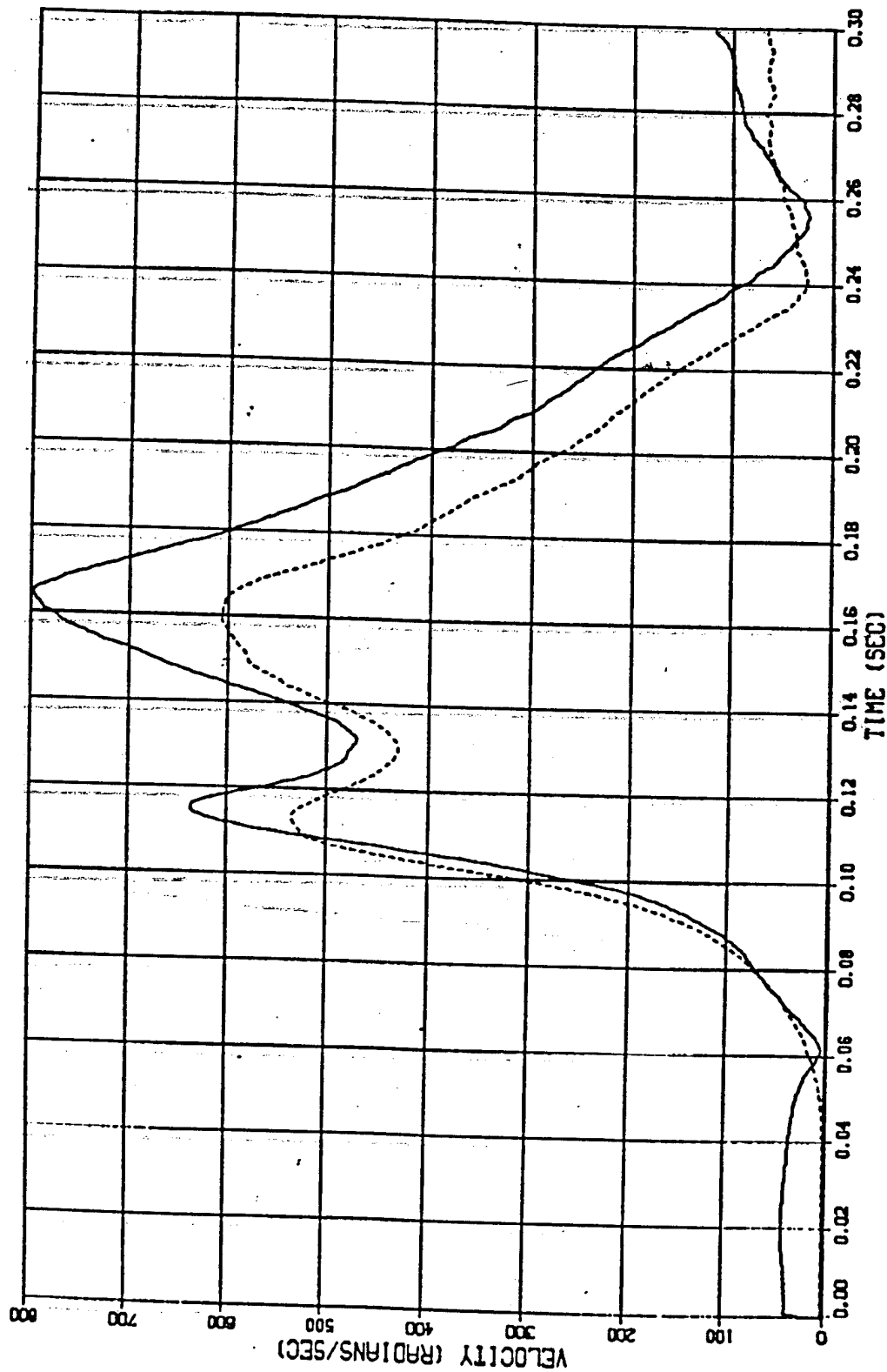


Fig 61



Figure 7. Axial Force Time-Course Comparisons for Subjects with Large (H132) and Small (H135) Heads Across Selected -X, +Y and -X+Y Impacts





AXIAL FORCE FOR MINUS X SLED DIRECTION

LEGEND

LX3982 FJCOXS H00132 15.61G
LX3970 FJCOXS H00135 15.55G

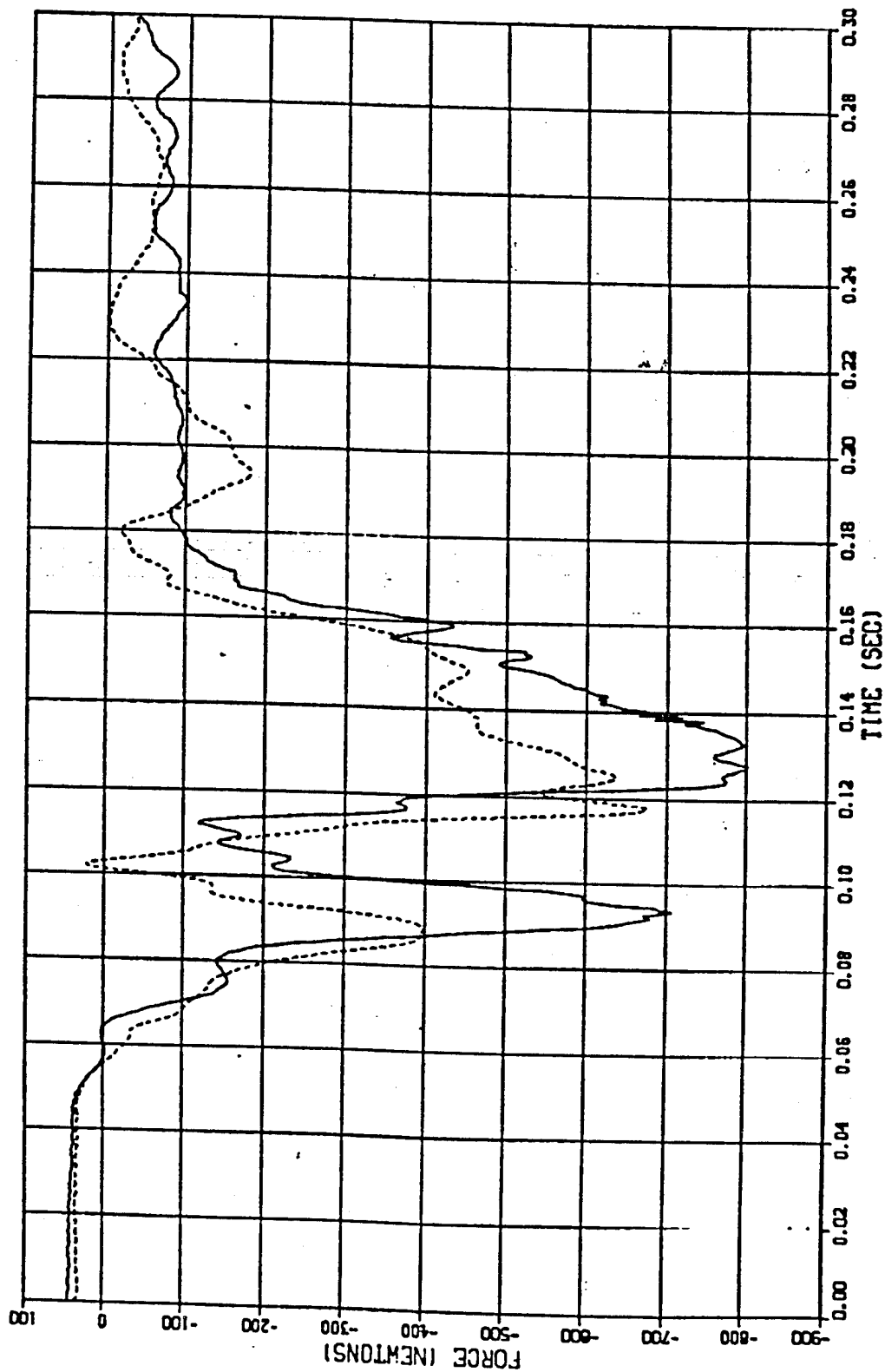


Fig 7a





AXIAL FORCE FOR PLUS Y SLED DIRECTION

LEGEND
LX4128 FJCOXS H00132 7.14G
LX4131 FJCOXS H00135 7.25G

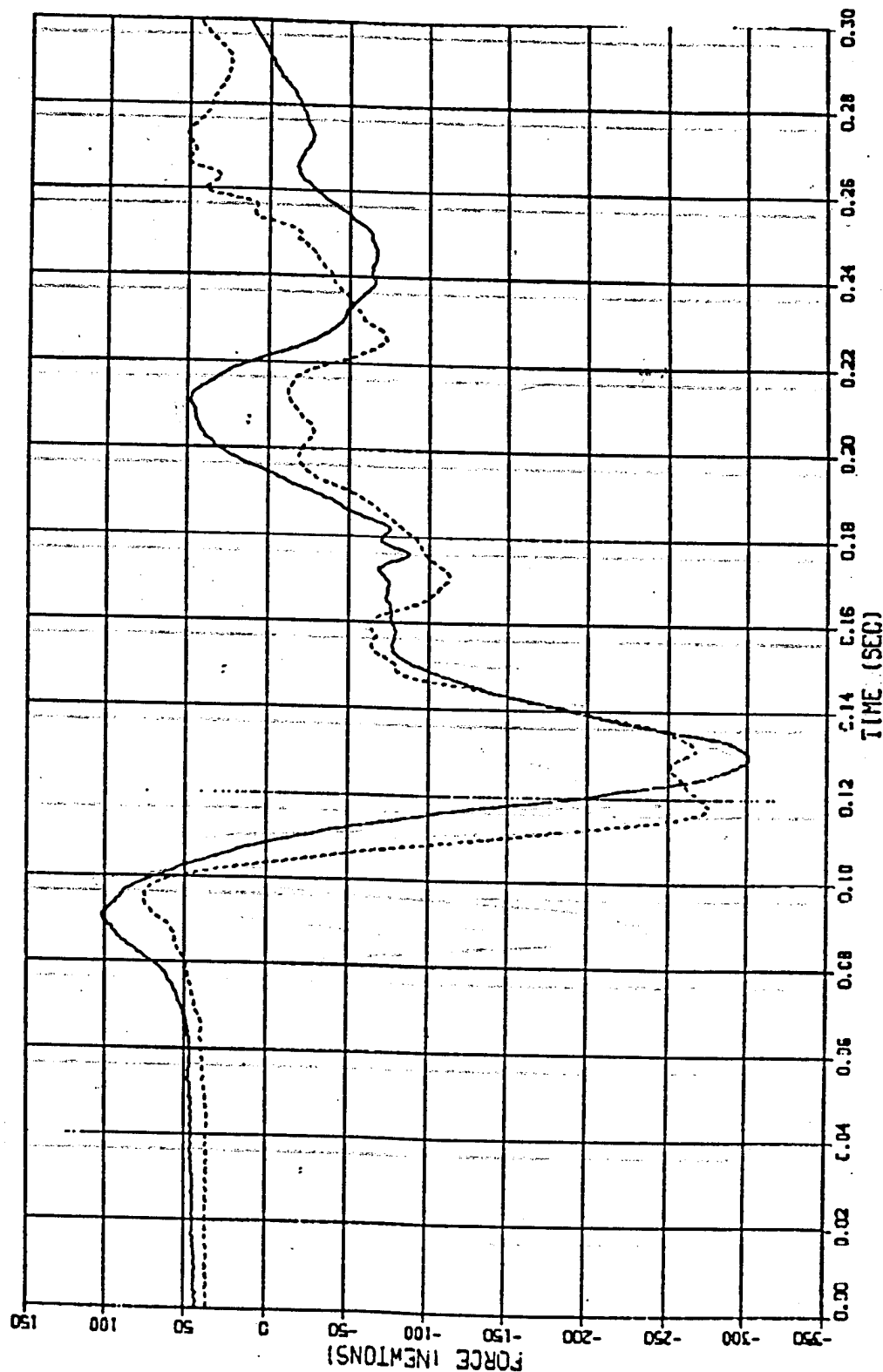


Fig 7b



AXIAL FORCE FOR MINUS X : PLUS Y SLED RUNS

LEGEND

LX4297 FJCXS H00132 10.03G
LX4316 FJCXS H00135 10.07G

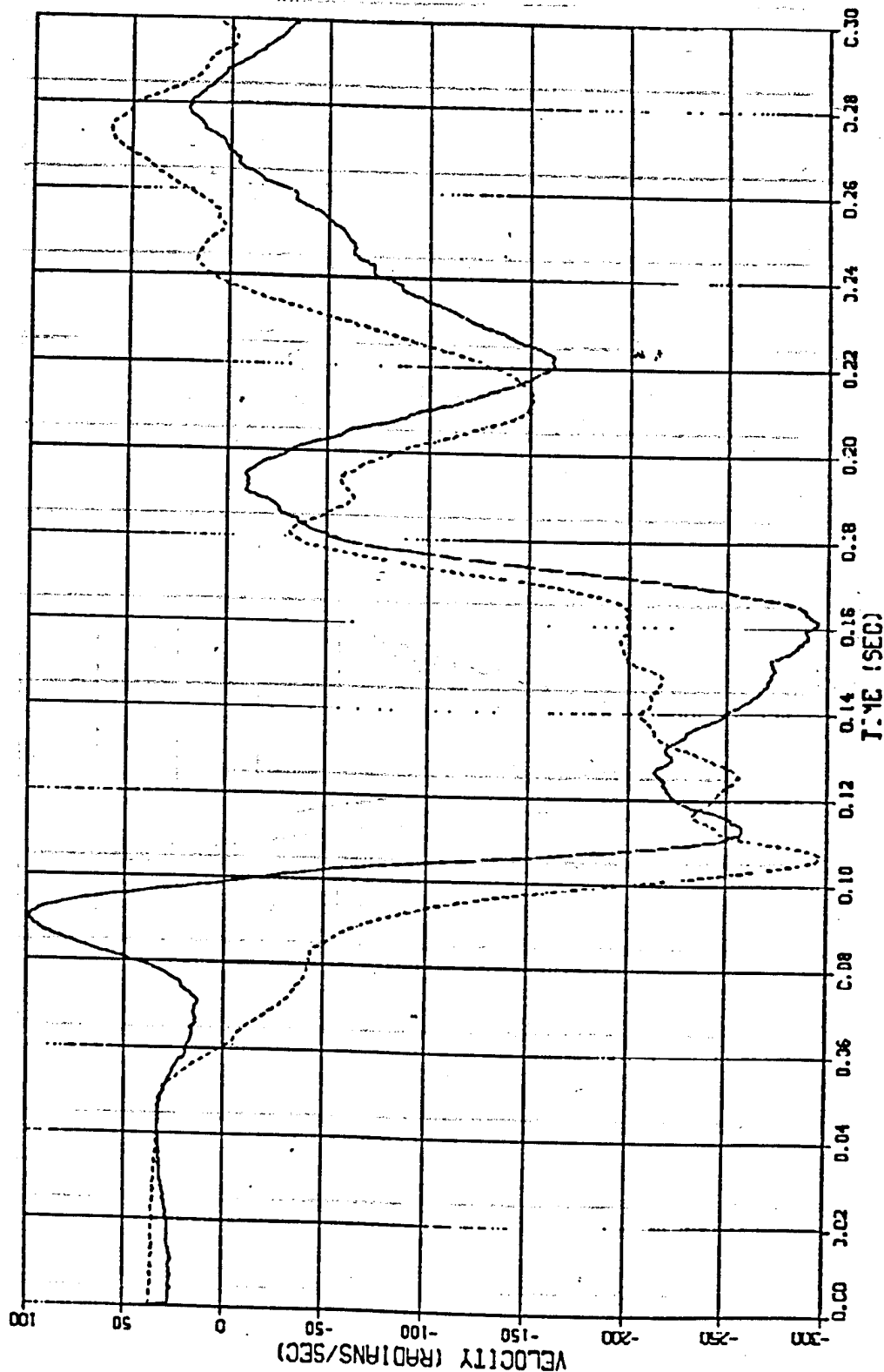


Fig 7c

AXIAL FORCE FOR MINUS X : PLUS Y SLED RUNS

LEGEND

LX4297 FJCOXS H00132 10.03G

LX4316 FJCOXS H00135 10.07G

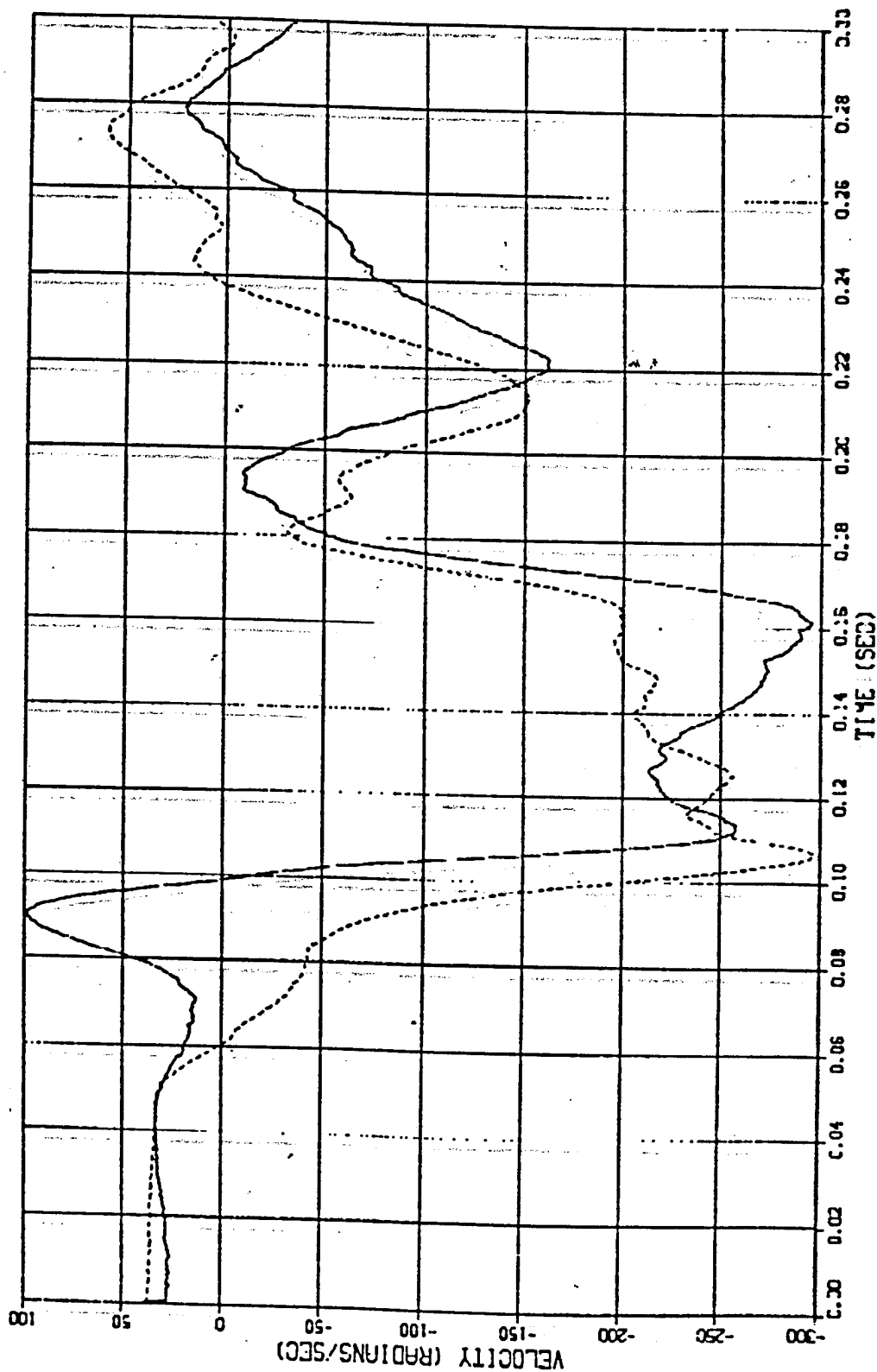


Figure 8. Resultant Torque Time-Course Comparisons for Subjects with Large (H132) and Small (H135) Heads Across -X, +Y and -X+Y Impacts



RESULTANT TORQUE FOR MINUS X SLED RUNS

LEGEND

LX3982 RJTORQ H00132 15.61G
LX3970 RJTORQ H00135 15.55G

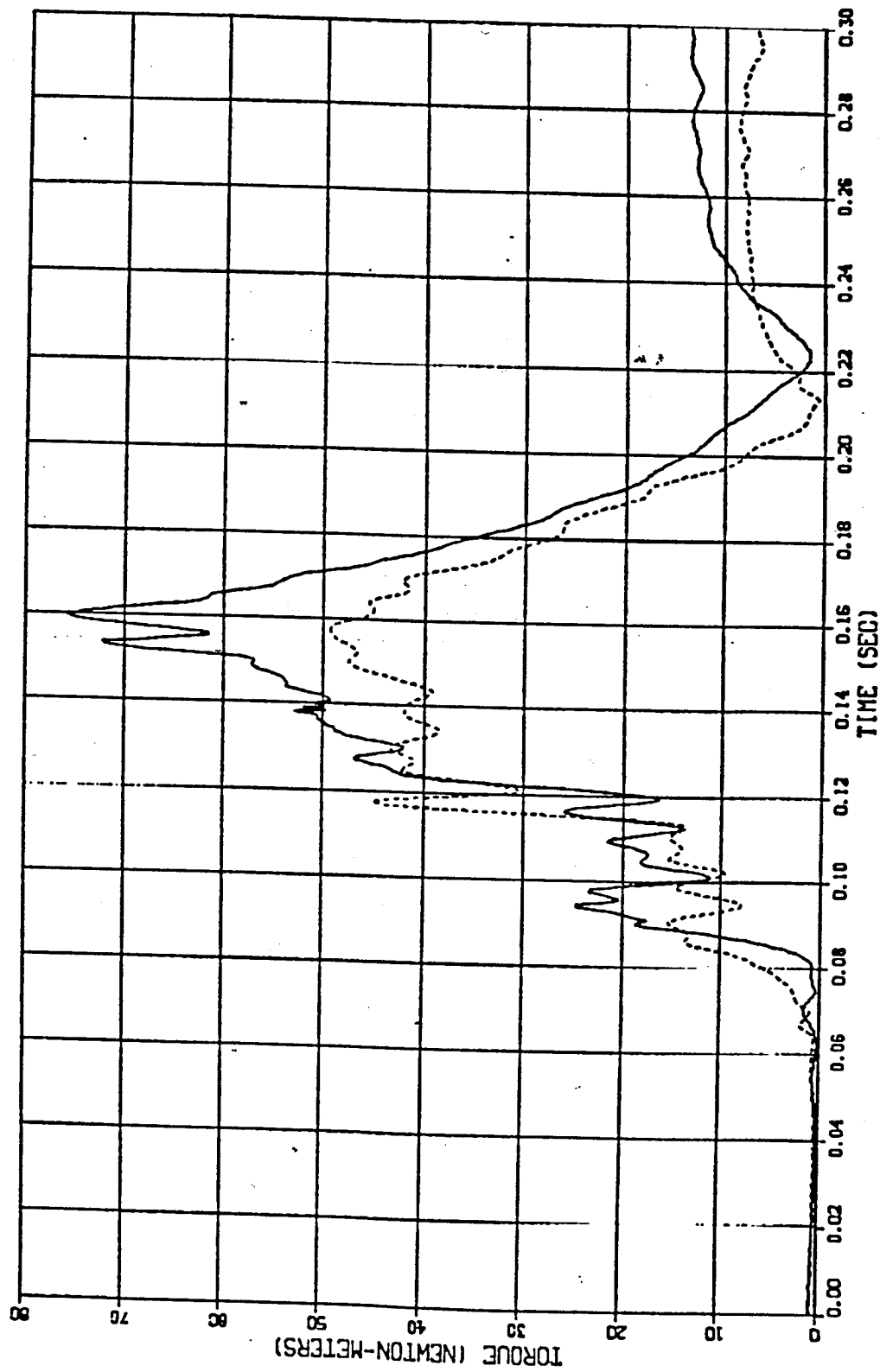


Fig 84





RESULTANT TORQUE FOR PLUS Y SLED RUNS

LEGEND

LX4128 RJTORQ H00132 7.14G
LX4131 RJTORQ H00135 7.25G

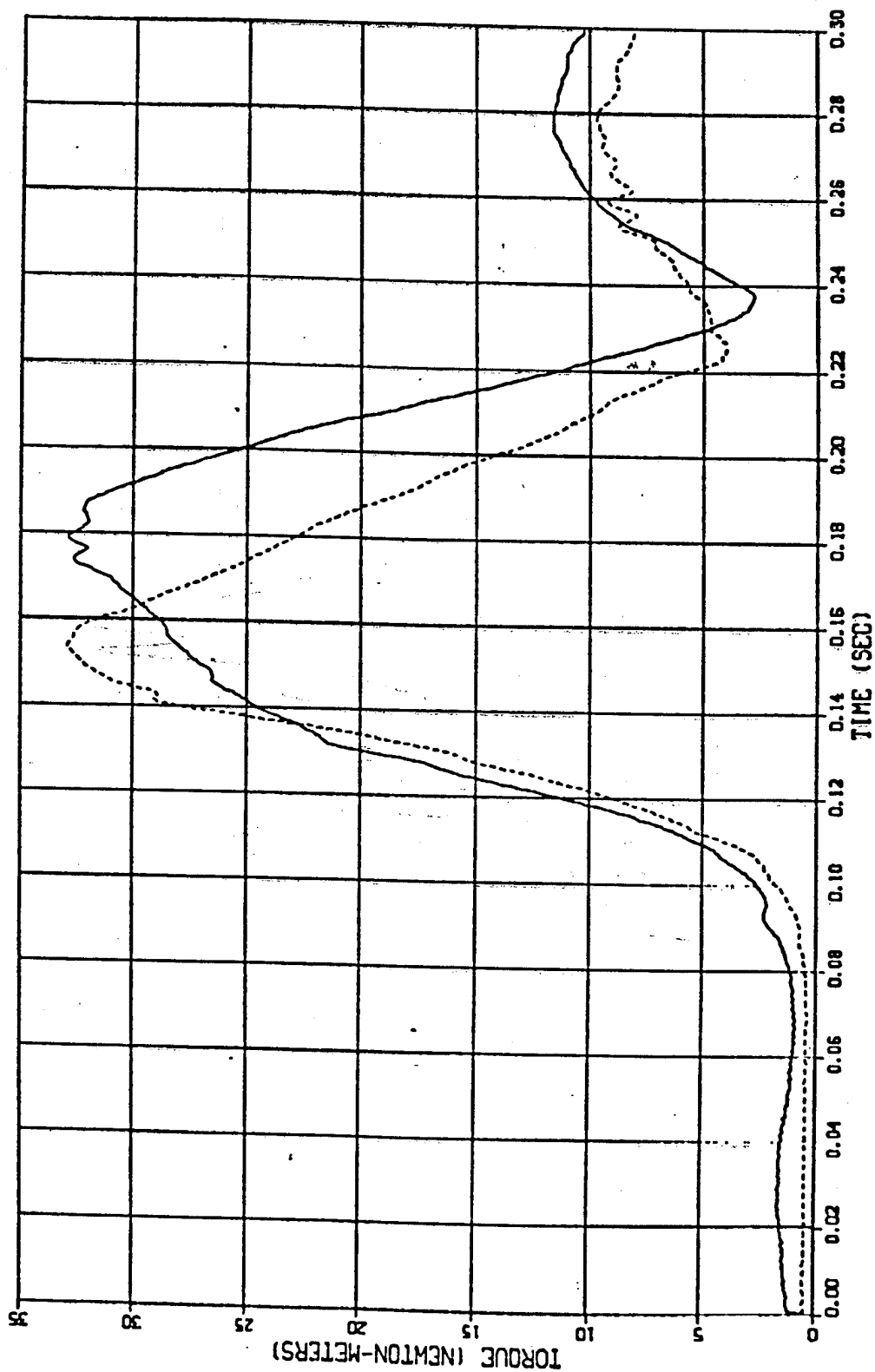
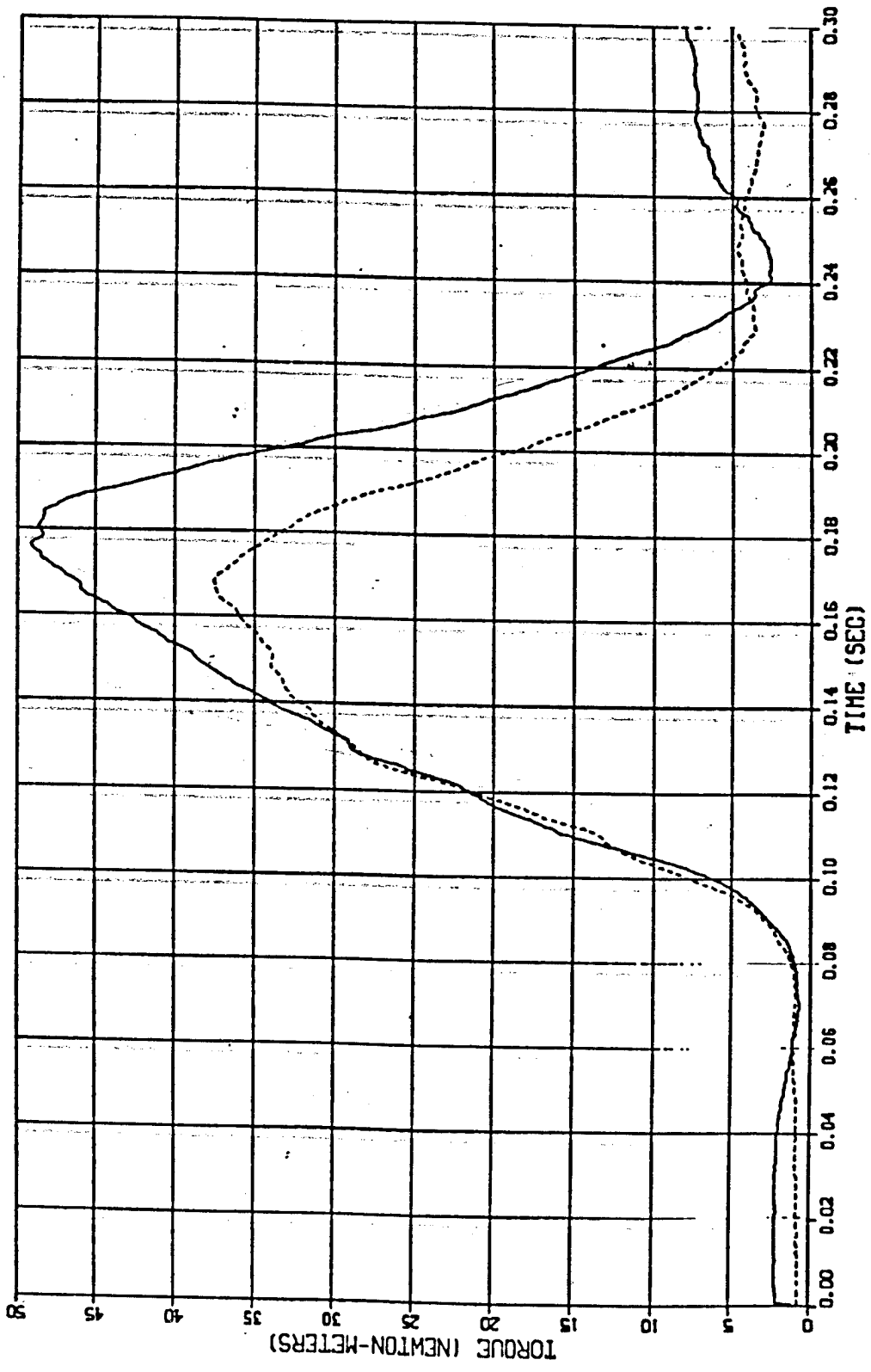


Fig 8b



RESULTANT TORQUE FOR MINUS X : PLUS Y SLED RUNS

LEGEND
 LX4297 RJTORQ HQ0132 10.03G
 LX4316 RJTORQ HQ0135 10.076



File DC

APPENDIX

SUBJECT (H131-H136) INJURY-RELATED VARIABLE SUMMARY TABLES FOR
SELECTED -X, +Y, AND -X+Y IMPACT ACCELERATIONS AT NBDL



SUBJECT H00131

*** Head Anatomical Configuration ***

Head Mass : 4.449 Kg.

Head Center of Gravity: X = +0.0084 Y = -0.0006 Z = +0.0317 Meters

Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters

Eigenvalues: 1 = +0.02198 2 = +0.02350 3 = +0.01529

Principal Axis Matrix
+0.82900 +0.00000 +0.55920
+0.00000 +1.00000 +0.00000
-0.55920 +0.00000 +0.82900

Moment of inertia matrix in A.C.S.
+0.019887 +0.000000 +0.003101
+0.000000 +0.023510 +0.000000
+0.003101 +0.000000 +0.017381

*** Minus X Sled Runs ***

| | 10 G-Level Run LX3908 | 13 G-Level Run LX3948 | 14 G-Level Run LX3987 | 15 G-Level Run LX3990 |
|--------------|--------------------------|--------------------------|--------------------------|--------------------------|
| | Max Min | Max Min | Max Min | Max Min |
| Force X-Axis | 140.59 -711.44 | 120.85 -828.81 | 139.87-1058.48 | 127.16 -982.90 |
| Force Y-Axis | 74.12 -76.47 | 26.99 77.77 | 56.72 -93.02 | 38.80 -131.41 |
| Force Z-Axis | 114.50 -404.53 | 44.34 -621.00 | 44.38 -721.15 | 45.03 -709.69 |
| Force Result | 788.51 4.63 | 980.34 15.66 | 1225.57 11.25 | 1180.26 14.98 |

| | 10 G-Level Run LX3993 | 13 G-Level Run LX3961 | 14 G-Level Run LX3968 87 | 15 G-Level Run LX3983 90 |
|---------------|--------------------------|--------------------------|-----------------------------|-----------------------------|
| | Max Min | Max Min | Max Min | Max Min |
| Torque X-Axis | 8.66 -6.95 | 6.70 -2.49 | 7.56 -4.38 | 10.90 -3.77 |
| Torque Y-Axis | 27.48 -45.81 | 11.48 -51.92 | 13.69 -58.89 | 13.10 -55.22 |
| Torque Z-Axis | 1.44 -2.96 | 0.89 -1.58 | 3.28 -3.55 | 2.56 -2.71 |
| Torque Result | 45.81 0.41 | 51.93 0.09 | 58.90 0.10 | 56.30 0.17 |

| | 10 G-Level Run LX3993 | 13 G-Level Run LX3961 | 14 G-Level Run LX3968 87 | 15 G-Level Run LX3983 90 ✓ |
|---------------|--------------------------|--------------------------|-----------------------------|-------------------------------|
| | HIC nbr Width | HIC nbr Width | HIC nbr Width | HIC nbr Width |
| HIC X-Axis | 47.77 80.00 | 84.55 76.50 | 114.03 75.00 | 112.08 74.50 |
| HIC Y-Axis | 0.03 150.50 | 0.04 160.00 | 0.16 93.00 | 0.24 91.00 |
| HIC Z-Axis | 9.33 61.50 | 14.81 53.50 | 19.79 47.50 | 21.08 44.00 |
| Resultant HIC | 65.33 114.00 | 112.04 94.50 | 153.53 83.50 | 155.58 83.00 |



SUBJECT H00131
*** Plus Y Sled Runs ***

| | 5 G-Level Run LX4089 | | 6 G-Level Run LX4109 | | 6 G-Level Run LX4138 | | 7 G-Level Run LX4124 | |
|--------------|-------------------------|---------|-------------------------|---------|-------------------------|---------|-------------------------|---------|
| | Max | Min | Max | Min | Max | Min | Max | Min |
| Force X-Axis | 43.83 | -213.44 | 63.95 | -218.45 | 58.28 | -192.78 | 50.69 | -190.52 |
| Force Y-Axis | 412.69 | -46.53 | 400.74 | -69.48 | 403.64 | -78.89 | 403.69 | -88.93 |
| Force Z-Axis | 54.85 | -198.98 | 53.97 | -309.86 | 75.07 | -241.51 | 69.86 | -323.39 |
| Force Result | 440.67 | 39.02 | 473.42 | 41.12 | 443.29 | 43.57 | 494.31 | 39.76 |

| | 5 G-Level Run LX4089 | | 6 G-Level Run LX4109 | | 6 G-Level Run LX4138 | | 7 G-Level Run LX4124 | |
|---------------|-------------------------|--------|-------------------------|--------|-------------------------|--------|-------------------------|--------|
| | Max | Min | Max | Min | Max | Min | Max | Min |
| Torque X-Axis | 2.67 | -32.58 | 4.32 | -32.48 | 6.33 | -35.00 | 7.09 | -33.13 |
| Torque Y-Axis | 7.09 | -11.98 | 7.10 | -11.02 | 6.33 | -11.24 | 8.92 | -11.28 |
| Torque Z-Axis | 9.57 | -1.86 | 11.70 | -2.91 | 12.67 | -3.13 | 12.95 | -4.86 |
| Torque Result | 35.79 | 0.56 | 35.33 | 0.07 | 36.78 | .71 | 35.41 | 0.25 |

| | 5 G-Level Run LX4089 | | | 6 G-Level Run LX4109 | | | 6 G-Level Run LX4138 | | | 7 G-Level Run LX4124 | | |
|---------------|-------------------------|-----|--------|-------------------------|-----|--------|-------------------------|-----|--------|-------------------------|-----|-------|
| | HIC | nbr | Width | HIC | nbr | Width | HIC | nbr | Width | HIC | nbr | Width |
| HIC X-Axis | 11.95 | | 94.00 | 12.65 | | 94.00 | 10.85 | | 97.50 | 13.02 | | 84.50 |
| HIC Y-Axis | 0.24 | | 129.00 | 0.20 | | 130.00 | 0.52 | | 73.00 | 0.41 | | 68.00 |
| HIC Z-Axis | 1.19 | | 59.50 | 2.59 | | 64.00 | 3.18 | | 67.00 | 2.66 | | 60.00 |
| Resultant HIC | 15.28 | | 95.00 | 17.85 | | 101.50 | 16.92 | | 107.50 | 18.09 | | 94.00 |

*** Minus X / Plus Y ***

| | 7 G-Level Run LX4242 | | 10 G-Level Run LX4251 | |
|--------------|-------------------------|---------|--------------------------|---------|
| | Max | Min | Max | Min |
| Force X-Axis | 6.81 | -395.81 | 98.05 | -700.19 |
| Force Y-Axis | 274.63 | -2.14 | 394.24 | -81.61 |
| Force Z-Axis | 51.17 | -155.54 | 42.81 | -467.41 |
| Force Result | 479.87 | 22.17 | 877.93 | 21.56 |

| | 7 G-Level Run LX4242 | | 10 G-Level Run LX4251 | |
|---------------|-------------------------|--------|--------------------------|--------|
| | Max | Min | Max | Min |
| Torque X-Axis | 0.20 | -20.71 | 6.91 | -28.93 |
| Torque Y-Axis | 0.76 | -27.23 | 7.37 | -44.60 |
| Torque Z-Axis | 7.71 | -2.34 | 12.52 | -5.17 |
| Torque Result | 31.48 | 0.17 | 51.52 | 0.35 |

| | 7 G-Level Run LX4242 | | | 10 G-Level Run LX4251 | | |
|---------------|-------------------------|-----|--------|--------------------------|-----|--------|
| | HIC | nbr | Width | HIC | nbr | Width |
| HIC X-Axis | 15.87 | | 104.00 | 55.08 | | 69.50 |
| HIC Y-Axis | 0.13 | | 77.00 | 2.15 | | 54.00 |
| HIC Z-Axis | 3.50 | | 67.50 | 13.18 | | 57.50 |
| Resultant HIC | 22.42 | | 113.00 | 83.28 | | 106.50 |



SUBJECT H00132

*** Head Anatomical Configuration ***

Head Mass : 4.523 Kg.
 Head Center of Gravity: X = +0.0084 Y = -0.0006 Z = +0.0318 Meters
 Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters
 Eigenvalues: 1 = +0.02259 2 = +0.02415 3 = +0.01572

| Principal Axis Matrix | | | Moment of inertia matrix in A.C.S. | | |
|-----------------------|----------|----------|------------------------------------|-----------|-----------|
| +0.82900 | +0.00000 | +0.55920 | +0.020440 | +0.000000 | +0.003185 |
| +0.00000 | +1.00000 | +0.00000 | +0.000000 | +0.024150 | +0.000000 |
| -0.55920 | +0.00000 | +0.82900 | +0.003185 | +0.000000 | +0.017867 |

*** Minus X Sled Runs ***

| | | 10 G-Level Run LX3989 | | 13 G-Level Run LX3950 | | 14 G-Level Run LX3957 | | 15 G-Level Run LX3982 | |
|-------|--------|--------------------------|---------|--------------------------|----------|--------------------------|----------|--------------------------|----------|
| | | Max | Min | Max | Min | Max | Min | Max | Min |
| Force | X-Axis | 55.43 | -691.57 | 118.72 | -1535.00 | 110.60 | -1199.90 | 143.99 | -1395.33 |
| Force | Y-Axis | 11.89 | -88.28 | 64.71 | -194.54 | 45.75 | -177.12 | 23.92 | -214.45 |
| Force | Z-Axis | 80.33 | -317.61 | 42.95 | -983.66 | 44.89 | -629.76 | 44.56 | -801.69 |
| Force | Result | 750.09 | 22.59 | 1823.22 | 4.61 | 1252.74 | 16.66 | 1514.52 | 8.89 |

| | | 10 G-Level Run LX3989 | | 13 G-Level Run LX3950 | | 14 G-Level Run LX3957 | | 15 G-Level Run LX3982 | |
|--------|--------|--------------------------|--------|--------------------------|--------|--------------------------|--------|--------------------------|--------|
| | | Max | Min | Max | Min | Max | Min | Max | Min |
| Torque | X-Axis | 6.39 | -0.86 | 11.19 | -15.49 | 7.80 | -3.22 | 11.73 | -6.22 |
| Torque | Y-Axis | 4.54 | -39.89 | 18.17 | -68.34 | 11.66 | -56.12 | 13.58 | -75.11 |
| Torque | Z-Axis | 0.62 | -3.00 | 7.42 | -4.79 | 2.59 | -5.25 | 1.23 | -4.15 |
| Torque | Result | 40.37 | 0.10 | 68.58 | 0.11 | 56.59 | 0.34 | 75.71 | 0.11 |

| | | 10 G-Level HIC nbr Width Run LX3989 | | 13 G-Level HIC nbr Width Run LX3950 | | 14 G-Level HIC nbr Width Run LX3957 | | 15 G-Level HIC nbr Width Run LX3982 | |
|---------------|--------|---|--------|---|--------|---|--------|---|-------|
| HIC | X-Axis | 40.62 | 81.50 | 93.49 | 72.50 | 118.32 | 74.50 | 112.06 | 65.00 |
| HIC | Y-Axis | 0.02 | 184.00 | 0.24 | 187.00 | 0.11 | 212.00 | 0.08 | 66.50 |
| HIC | Z-Axis | 6.25 | 75.50 | 16.61 | 19.50 | 13.42 | 41.00 | 29.03 | 41.00 |
| Resultant HIC | | 50.01 | 94.50 | 126.49 | 83.50 | 146.99 | 81.00 | 167.47 | 83.00 |



SUBJECT H00132
*** Plus Y Sled Runs ***

| | 5 G-Level Run LX4090 | | 6 G-Level Run LX4110 | | 7 G-Level Run LX4128 | |
|--------------|-------------------------|---------|-------------------------|---------|-------------------------|---------|
| | Max | Min | Max | Min | Max | Min |
| Force X-Axis | 42.26 | -178.27 | 35.75 | -315.75 | 60.02 | -287.66 |
| Force Y-Axis | 291.58 | -19.82 | 414.47 | -89.96 | 392.60 | -138.20 |
| Force Z-Axis | 77.41 | -168.80 | 73.51 | -320.10 | 101.81 | -301.20 |
| Force Result | 343.08 | 38.09 | 539.94 | 28.51 | 495.36 | 44.30 |

| | 5 G-Level Run LX4090 | | 6 G-Level Run LX4110 | | 7 G-Level Run LX4128 | |
|---------------|-------------------------|--------|-------------------------|--------|-------------------------|--------|
| | Max | Min | Max | Min | Max | Min |
| Torque X-Axis | 1.92 | -19.70 | 7.49 | -29.34 | 10.84 | -27.67 |
| Torque Y-Axis | 3.46 | -8.27 | 5.56 | -13.79 | 5.33 | -15.05 |
| Torque Z-Axis | 8.00 | -1.32 | 11.35 | -2.96 | 13.85 | -3.81 |
| Torque Result | 22.49 | 0.23 | 33.73 | 0.27 | 32.89 | 0.26 |

| | 5 G-Level Run LX4090 | | 6 G-Level Run LX4110 | | 7 G-Level Run LX4128 | |
|---------------|-------------------------|--------|-------------------------|--------|-------------------------|--------|
| | HIC nbr | Width | HIC nbr | Width | HIC nbr | Width |
| HIC X-Axis | 5.94 | 124.00 | 14.78 | 101.00 | 12.53 | 94.00 |
| HIC Y-Axis | 0.09 | 214.50 | 0.23 | 26.50 | 0.13 | 216.00 |
| HIC Z-Axis | 1.74 | 80.00 | 2.01 | 54.00 | 3.69 | 61.00 |
| Resultant HIC | 9.01 | 137.50 | 19.71 | 104.00 | 18.77 | 104.50 |

*** Minus X / Plus Y ***

| | 7 G-Level Run LX4261 | | 10 G-Level Run LX4297 | | 11 G-Level Run LX4306 | |
|--------------|-------------------------|---------|--------------------------|---------|--------------------------|---------|
| | Max | Min | Max | Min | Max | Min |
| Force X-Axis | 26.95 | -568.61 | 64.44 | -752.94 | 31.41 | -713.83 |
| Force Y-Axis | 299.74 | -60.54 | 311.01 | -104.52 | 341.89 | -74.08 |
| Force Z-Axis | 44.64 | -202.31 | 98.66 | -295.38 | 45.72 | -301.87 |
| Force Result | 650.44 | 14.79 | 848.15 | 17.48 | 834.00 | 26.42 |

| | 7 G-Level Run LX4261 | | 10 G-Level Run LX4297 | | 11 G-Level Run LX4306 | |
|---------------|-------------------------|--------|--------------------------|--------|--------------------------|--------|
| | Max | Min | Max | Min | Max | Min |
| Torque X-Axis | 4.35 | -20.38 | 6.62 | -18.26 | 4.00 | -21.82 |
| Torque Y-Axis | 2.03 | -35.51 | 5.30 | -45.39 | 3.26 | -46.70 |
| Torque Z-Axis | 8.88 | -1.31 | 10.91 | -4.28 | 10.06 | -2.59 |
| Torque Result | 40.70 | 0.46 | 49.07 | 0.52 | 51.65 | 0.62 |

| | 7 G-Level Run LX4261 | | 10 G-Level Run LX4297 | | 11 G-Level Run LX4306 | |
|---------------|-------------------------|--------|--------------------------|-------|--------------------------|-------|
| | HIC nbr | Width | HIC nbr | Width | HIC nbr | Width |
| HIC X-Axis | 36.62 | 103.50 | 45.65 | 77.00 | 50.09 | 84.00 |
| HIC Y-Axis | 0.46 | 44.00 | 1.22 | 32.50 | 0.57 | 28.00 |
| HIC Z-Axis | 3.15 | 56.50 | 7.04 | 53.50 | 8.83 | 53.00 |
| Resultant HIC | 45.72 | 108.50 | 60.14 | 95.00 | 66.50 | 95.50 |



SUBJECT H00133

*** Head Anatomical Configuration ***

Head Mass : 4.170 Kg.
 Head Center of Gravity: X = +0.0082 Y = -0.0005 Z = +0.0310 Meters
 Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters
 Eigenvalues: 1 = +0.01973 2 = +0.02110 3 = +0.01373

| Principal Axis Matrix | | | Moment of inertia matrix in A.C.S. | | |
|-----------------------|----------|----------|------------------------------------|-----------|-----------|
| +0.82900 | +0.00000 | +0.55920 | +0.017853 | +0.000000 | +0.002781 |
| +0.00000 | +1.00000 | +0.00000 | +0.000000 | +0.021100 | +0.000000 |
| -0.55920 | +0.00000 | +0.82900 | +0.002781 | +0.000000 | +0.015605 |

*** Minus X Sled Runs ***

| | 10 G-Level Run LX3998 | 13 G-Level Run LX3951 | 14 G-Level Run LX3963 | 15 G-Level Run LX3986 |
|--------------|--------------------------|--------------------------|--------------------------|--------------------------|
| | Max Min | Max Min | Max Min | Max Min |
| Force X-Axis | 96.70 -757.19 | 96.06 -855.84 | 115.21 -867.71 | 53.09 -552.93 |
| Force Y-Axis | 34.28 -78.60 | 70.55 -142.20 | 85.05 -149.16 | 26.64 -99.08 |
| Force Z-Axis | 40.77 -740.92 | 40.78 -726.01 | 40.65 -867.30 | 83.78 -414.60 |
| Force Result | 978.92 4.99 | 1122.77 11.35 | 1147.43 10.67 | 671.05 2.96 |

| | 10 G-Level Run LX3998 | 13 G-Level Run LX3951 | 14 G-Level Run LX3963 | 15 G-Level Run LX3986 |
|---------------|--------------------------|--------------------------|--------------------------|--------------------------|
| | Max Min | Max Min | Max Min | Max Min |
| Torque X-Axis | 9.22 -2.39 | 6.14 -4.61 | 13.39 -8.25 | 9.22 -2.39 |
| Torque Y-Axis | 3.14 -38.31 | 9.29 -48.99 | 11.65 -55.96 | 3.14 -38.31 |
| Torque Z-Axis | 1.34 -1.47 | 4.11 -3.40 | 3.96 -3.10 | 1.34 -1.47 |
| Torque Result | 39.15 0.15 | 49.06 0.03 | 56.19 0.13 | 39.15 0.15 |

| | 10 G-Level Run LX3998 | 13 G-Level Run LX3951 | 14 G-Level Run LX3963 | 15 G-Level Run LX3986 |
|---------------|--------------------------|--------------------------|--------------------------|--------------------------|
| | HIC nbr Width | HIC nbr Width | HIC nbr Width | HIC nbr Width |
| HIC X-Axis | 43.28 97.00 | 86.99 76.50 | 96.61 77.50 | 131.30 77.00 |
| HIC Y-Axis | 0.06 73.00 | 0.06 216.00 | 0.09 144.00 | 0.20 77.50 |
| HIC Z-Axis | 5.11 62.50 | 17.29 48.00 | 15.57 50.50 | 23.83 41.50 |
| Resultant HIC | 55.32 106.50 | 120.17 94.00 | 125.77 89.00 | 177.62 88.50 |



SUBJECT H00133
*** Plus Y Sled Runs ***

| | | 5 G-Level | | 6 G-Level | | 7 G-Level | |
|-------|--------|------------|---------|------------|---------|------------|---------|
| | | Run LX4093 | | Run LX4111 | | Run LX4125 | |
| | | Max | Min | Max | Min | Max | Min |
| Force | X-Axis | 43.51 | -163.40 | 27.00 | -188.44 | 24.50 | -274.48 |
| Force | Y-Axis | 364.71 | -34.23 | 395.26 | -51.60 | 577.36 | -108.84 |
| Force | Z-Axis | 47.67 | -159.00 | 71.89 | -276.20 | 68.77 | -369.02 |
| Force | Result | 380.65 | 40.25 | 444.90 | 30.88 | 647.16 | 36.46 |

| | | 5 G-Level | | 6 G-Level | | 7 G-Level | |
|--------|--------|------------|--------|------------|--------|------------|--------|
| | | Run LX4093 | | Run LX4111 | | Run LX4125 | |
| | | Max | Min | Max | Min | Max | Min |
| Torque | X-Axis | 2.84 | -28.16 | 3.91 | -33.20 | 8.71 | -44.60 |
| Torque | Y-Axis | 4.70 | -10.12 | 3.30 | -9.25 | 4.26 | -12.65 |
| Torque | Z-Axis | 9.38 | -0.27 | 10.32 | -1.15 | 16.68 | -2.43 |
| Torque | Result | 30.38 | 0.49 | 35.42 | 0.69 | 49.05 | 0.64 |

| | | 5 G-Level | | 6 G-Level | | 7 G-Level | |
|---------------|--------|------------|--------|------------|--------|------------|-------|
| | | Run LX4093 | | Run LX4111 | | Run LX4125 | |
| | | HIC nbr | Width | HIC nbr | Width | HIC nbr | Width |
| HIC | X-Axis | 11.62 | 104.50 | 16.36 | 97.00 | 24.85 | 74.00 |
| HIC | Y-Axis | 0.18 | 148.50 | 0.25 | 135.00 | 0.23 | 79.50 |
| HIC | Z-Axis | 0.63 | 268.00 | 1.72 | 61.50 | 3.95 | 44.00 |
| Resultant HIC | | 13.74 | 106.00 | 21.05 | 102.50 | 32.93 | 78.50 |

*** Minus X / Plus Y ***

| | | 7 G-Level | | 10 G-Level | |
|-------|--------|------------|---------|------------|---------|
| | | Run LX4236 | | Run LX4240 | |
| | | Max | Min | Max | Min |
| Force | X-Axis | 3.74 | -343.93 | 11.38 | -447.93 |
| Force | Y-Axis | 338.00 | -8.19 | 499.11 | -39.79 |
| Force | Z-Axis | 45.92 | -159.02 | 52.51 | -273.00 |
| Force | Result | 497.62 | 213.34 | 643.11 | 12.44 |

| | | 7 G-Level | | 10 G-Level | |
|--------|--------|------------|--------|------------|--------|
| | | Run LX4236 | | Run LX4240 | |
| | | Max | Min | Max | Min |
| Torque | X-Axis | 1.84 | -22.29 | 2.80 | -26.65 |
| Torque | Y-Axis | 0.34 | -20.87 | 0.80 | -25.14 |
| Torque | Z-Axis | 9.18 | -0.11 | 11.45 | -0.94 |
| Torque | Result | 31.33 | 0.09 | 36.51 | 0.22 |

| | | 7 G-Level | | 10 G-Level | |
|---------------|--------|------------|--------|------------|--------|
| | | Run LX4236 | | Run LX4240 | |
| | | HIC nbr | Width | HIC nbr | Width |
| HIC | X-Axis | 26.26 | 107.50 | 39.86 | 104.50 |
| HIC | Y-Axis | 0.18 | 45.50 | 0.33 | 44.50 |
| HIC | Z-Axis | 1.04 | 115.00 | 3.98 | 57.50 |
| Resultant HIC | | 29.97 | 108.50 | 50.50 | 106.50 |



SUBJECT H00134

*** Head Anatomical Configuration ***

Head Mass : 4.278 Kg.

Head Center of Gravity: X = +0.0083 Y = -0.0005 Z = +0.0313 Meters

Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters

Eigenvalues: 1 = +0.02059 2 = +0.02201 3 = +0.01433

Principal Axis Matrix

+0.82900 +0.00000 +0.55920
+0.00000 +1.00000 +0.00000
-0.55920 +0.00000 +0.82900

Moment of inertia matrix in A.C.S.

+0.018631 +0.000000 +0.002902
+0.000000 +0.022010 +0.000000
+0.002902 +0.000000 +0.016287

*** Minus X Sled Runs ***

| | 10 G-Level Run LX3993 | 13 G-Level Run LX3961 | 14 G-Level Run LX3968 | 15 G-Level Run LX3983 |
|--------------|--------------------------|--------------------------|--------------------------|--------------------------|
| | Max Min | Max Min | Max Min | Max Min |
| Force X-Axis | 28.56 -629.12 | 81.13 -969.39 | 92.79 -961.99 | 100.82 -994.27 |
| Force Y-Axis | 20.05 -42.76 | 30.54 -84.36 | 57.22 -119.35 | 67.90 -89.18 |
| Force Z-Axis | 46.41 -418.24 | 41.61 -739.49 | 43.32 -826.82 | 42.62 -769.25 |
| Force Result | 722.41 14.38 | 1089.09 +11.57 | 1114.39 13.86 | 1182.19 10.44 |

| | 10 G-Level Run LX3993 | 13 G-Level Run LX3961 | 14 G-Level Run LX3968 | 15 G-Level Run LX3983 |
|---------------|--------------------------|--------------------------|--------------------------|--------------------------|
| | Max Min | Max Min | Max Min | Max Min |
| Torque X-Axis | 3.77 -1.98 | 5.67 -1.91 | 7.27 -5.35 | 7.75 -3.02 |
| Torque Y-Axis | 2.06 -39.14 | 7.09 -47.83 | 10.04 -53.65 | 9.23 -55.22 |
| Torque Z-Axis | 0.63 -0.68 | 1.50 -2.65 | 2.39 -4.18 | 1.05 -1.71 |
| Torque Result | 39.25 +0.05 | 47.99 +0.05 | 53.72 +0.02 | 55.76 0.15 |

| | 10 G-Level Run LX3993 | 13 G-Level Run LX3961 | 14 G-Level Run LX3968 | 15 G-Level Run LX3983 |
|---------------|--------------------------|--------------------------|--------------------------|--------------------------|
| | HIC Nbr Width | HIC Nbr Width | HIC Nbr Width | HIC Nbr Width |
| HIC X-Axis | 46.27 80.00 | 96.30 67.50 | 93.33 67.00 | 137.66 71.50 |
| HIC Y-Axis | 0.08 89.00 | 0.64 200.50 | 0.11 121.00 | 0.22 175.00 |
| HIC Z-Axis | 10.54 65.00 | 18.36 54.50 | 25.43 49.50 | 25.01 43.00 |
| Resultant HIC | 66.03 103.00 | 127.56 89.00 | 134.16 87.00 | 186.80 84.00 |



SUBJECT H00134
*** Plus Y Sled Runs ***

| | 5 G-Level Run LX4097 | | 6 G-Level Run LX4112 | | 7 G-Level Run LX4126 | |
|--------------|-------------------------|---------|-------------------------|---------|-------------------------|---------|
| | Max | Min | Max | Min | Max | Min |
| Force X-Axis | 20.59 | -171.14 | 31.85 | -243.86 | 60.02 | -262.26 |
| Force Y-Axis | 330.00 | -42.60 | 366.24 | -67.13 | 399.14 | -87.26 |
| Force Z-Axis | 43.97 | -162.33 | 52.70 | -250.91 | 47.34 | -307.52 |
| Force Result | 374.40 | 16.35 | 422.86 | 31.73 | 489.36 | 41.01 |

| | 5 G-Level Run LX4097 | | 6 G-Level Run LX4112 | | 7 G-Level Run LX4126 | |
|---------------|-------------------------|--------|-------------------------|--------|-------------------------|--------|
| | Max | Min | Max | Min | Max | Min |
| Torque X-Axis | 2.77 | -24.35 | 5.53 | -31.37 | 6.92 | -31.04 |
| Torque Y-Axis | 2.25 | -10.17 | 4.14 | -14.51 | 8.02 | -14.86 |
| Torque Z-Axis | 7.90 | -0.25 | 10.94 | -2.23 | 10.66 | -2.81 |
| Torque Result | 26.57 | +0.34 | 33.02 | +0.45 | 34.45 | +0.04 |

| | 5 G-Level Run LX4097 | | 6 G-Level Run LX4112 | | 7 G-Level Run LX4126 | |
|---------------|-------------------------|--------|-------------------------|--------|-------------------------|--------|
| | HIC Nbr | Width | HIC Nbr | Width | HIC Nbr | Width |
| HIC X-Axis | 11.15 | 114.50 | 13.69 | 103.50 | 16.27 | 86.50 |
| HIC Y-Axis | 0.08 | 133.00 | 0.06 | 143.50 | 0.21 | 112.00 |
| HIC Z-Axis | 1.14 | 70.00 | 0.98 | 69.50 | 2.08 | 55.00 |
| Resultant HIC | 13.70 | 116.50 | 15.89 | 105.50 | 20.62 | 91.00 |

*** Minus X / Plus Y ***

| | 9 G-Level Run LX4264 | | 10 G-Level Run LX4298 | | 11 G-Level Run LX4307 | |
|--------------|-------------------------|---------|--------------------------|---------|--------------------------|---------|
| | Max | Min | Max | Min | Max | Min |
| Force X-Axis | 30.28 | -520.00 | 37.18 | -589.15 | 43.68 | -680.55 |
| Force Y-Axis | 356.98 | -48.65 | 341.57 | -49.29 | 361.52 | -86.75 |
| Force Z-Axis | 42.31 | -337.14 | 43.75 | -473.28 | 42.29 | -631.21 |
| Force Result | 681.84 | 25.56 | 755.83 | +14.07 | 924.77 | 12.78 |

| | 9 G-Level Run LX4264 | | 10 G-Level Run LX4298 | | 11 G-Level Run LX4307 | |
|---------------|-------------------------|--------|--------------------------|--------|--------------------------|--------|
| | Max | Min | Max | Min | Max | Min |
| Torque X-Axis | 4.33 | -28.12 | 3.69 | -23.99 | 6.58 | -29.66 |
| Torque Y-Axis | 2.47 | -32.52 | 3.15 | -36.92 | 3.69 | -42.53 |
| Torque Z-Axis | 10.54 | -0.90 | 10.82 | -1.49 | 12.12 | -0.88 |
| Torque Result | 41.17 | +0.06 | 42.17 | +0.17 | 48.55 | +0.03 |

| | 9 G-Level Run LX4264 | | 10 G-Level Run LX4298 | | 11 G-Level Run LX4307 | |
|---------------|-------------------------|--------|--------------------------|--------|--------------------------|--------|
| | HIC Nbr | Width | HIC Nbr | Width | HIC Nbr | Width |
| HIC X-Axis | 40.91 | 82.50 | 45.56 | 74.50 | 70.22 | 75.00 |
| HIC Y-Axis | 0.35 | 188.00 | 0.23 | 142.00 | 0.66 | 196.00 |
| HIC Z-Axis | 5.30 | 114.00 | 8.85 | 63.00 | 12.53 | 105.50 |
| Resultant HIC | 54.40 | 107.00 | 62.68 | 102.00 | 96.89 | 87.00 |



SUBJECT H00135

*** Head Anatomical Configuration ***

Head Mass : 3.791 Kg.

Head Center of Gravity: X = +0.0080 Y = -0.0005 Z = +0.0300 Meters

Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters

Eigenvalues: 1 = +0.01683 2 = +0.01800 3 = +0.01171

Principal Axis Matrix

+0.82900 +0.00000 +0.55920
+0.00000 +1.00000 +0.00000
-0.55920 +0.00000 +0.82900

Moment of inertia matrix in A.C.S.

+0.015228 +0.000000 +0.002374
+0.000000 +0.018000 +0.000000
+0.002374 +0.000000 +0.013310

*** Minus X Sled Runs ***

| | 10 G-Level Run LX3916 | | 13 G-Level Run LX3955 | | 14 G-Level Run LX3965 | | 15 G-Level Run LX3970 | |
|--------------|--------------------------|---------|--------------------------|---------|--------------------------|----------|--------------------------|---------|
| | Max | Min | Max | Min | Max | Min | Max | Min |
| Force X-Axis | 80.70 | -632.31 | 122.75 | -786.30 | 114.80 | -1078.20 | 91.83 | -840.30 |
| Force Y-Axis | 36.37 | -109.08 | 25.83 | -120.50 | 44.89 | -141.20 | 16.60 | -210.44 |
| Force Z-Axis | 71.48 | -360.26 | 114.49 | -559.82 | 192.81 | -764.17 | 36.55 | -675.56 |
| Force Result | 717.10 | 6.56 | 891.40 | 10.25 | 1294.03 | 11.38 | 955.28 | 9.40 |

| | 10 G-Level Run LX3916 | | 13 G-Level Run LX3955 | | 14 G-Level Run LX3965 | | 15 G-Level Run LX3970 | |
|---------------|--------------------------|--------|--------------------------|--------|--------------------------|--------|--------------------------|--------|
| | Max | Min | Max | Min | Max | Min | Max | Min |
| Torque X-Axis | 8.27 | -2.39 | 9.50 | -2.26 | 9.68 | -5.45 | 18.09 | -1.70 |
| Torque Y-Axis | 5.41 | -33.14 | 7.63 | -44.79 | 8.78 | -68.54 | 8.68 | -49.17 |
| Torque Z-Axis | 0.94 | -1.29 | 2.52 | -2.94 | 3.68 | -3.70 | 2.05 | -4.10 |
| Torque Result | 33.21 | 0.13 | 44.82 | 0.24 | 68.58 | 0.17 | 49.35 | 0.27 |

| | 10 G-Level Run LX3916 | | 13 G-Level Run LX3955 | | 14 G-Level Run LX3965 | | 15 G-Level Run LX3970 | |
|---------------|--------------------------|--------|--------------------------|--------|--------------------------|--------|--------------------------|--------|
| | HIC Nbr | Width | HIC Nbr | Width | HIC Nbr | Width | HIC Nbr | Width |
| HIC X-Axis | 50.13 | 85.50 | 90.27 | 75.50 | 116.77 | 74.00 | 109.17 | 75.50 |
| HIC Y-Axis | 0.08 | 38.50 | 0.06 | 200.00 | 0.24 | 207.00 | 0.06 | 229.00 |
| HIC Z-Axis | 9.27 | 137.00 | 16.62 | 49.50 | 23.61 | 108.50 | 24.95 | 45.00 |
| Resultant HIC | 66.22 | 107.50 | 120.46 | 87.50 | 162.35 | 84.00 | 154.17 | 86.50 |



SUBJECT H00135
*** Plus Y Sled Runs ***

| | 5 G-Level Run LX4095 | | 6 G-Level Run LX4114 | | 7 G-Level Run LX4131 | |
|--------------|-------------------------|---------|-------------------------|---------|-------------------------|---------|
| | Max | Min | Max | Min | Max | Min |
| Force X-Axis | 31.37 | -144.94 | 30.70 | -204.51 | 52.96 | -254.57 |
| Force Y-Axis | 286.25 | -61.93 | 329.41 | -91.10 | 365.60 | -120.51 |
| Force Z-Axis | 54.27 | -140.82 | 63.02 | -224.09 | 76.10 | -275.73 |
| Force Result | 325.10 | 30.09 | 375.44 | 32.69 | 447.19 | 36.17 |

| | 5 G-Level Run LX4095 | | 6 G-Level Run LX4114 | | 7 G-Level Run LX4131 | |
|---------------|-------------------------|--------|-------------------------|--------|-------------------------|--------|
| | Max | Min | Max | Min | Max | Min |
| Torque X-Axis | 5.34 | -21.65 | 6.21 | -23.75 | 8.84 | -28.43 |
| Torque Y-Axis | 3.07 | -8.76 | 3.55 | -9.52 | 7.36 | -12.95 |
| Torque Z-Axis | 7.75 | -1.17 | 7.91 | -1.94 | 10.66 | -3.03 |
| Torque Result | 23.96 | 0.23 | 26.48 | 0.27 | 32.92 | 0.33 |

| | 5 G-Level Run LX4095 | | 6 G-Level Run LX4114 | | 7 G-Level Run LX4131 | |
|---------------|-------------------------|--------|-------------------------|--------|-------------------------|--------|
| | HIC Nbr | Width | HIC Nbr | Width | HIC Nbr | Width |
| HIC X-Axis | 11.42 | 117.00 | 14.85 | 102.50 | 40.85 | 81.00 |
| HIC Y-Axis | 0.13 | 151.50 | 0.15 | 141.50 | 0.32 | 131.50 |
| HIC Z-Axis | 0.89 | 74.00 | 1.30 | 48.50 | 3.88 | 54.50 |
| Resultant HIC | 13.77 | 121.00 | 18.28 | 102.00 | 50.76 | 101.00 |

*** Minus X / Plus Y ***

| | 9 G-Level Run LX4314 | | 10 G-Level Run LX4316 | |
|--------------|-------------------------|-----|--------------------------|-----|
| | Max | Min | Max | Min |
| Force X-Axis | . | . | . | . |
| Force Y-Axis | . | . | . | . |
| Force Z-Axis | . | . | . | . |
| Force Result | . | . | . | . |

| | 9 G-Level Run LX4314 | | 10 G-Level Run LX4316 | |
|---------------|-------------------------|-----|--------------------------|-----|
| | Max | Min | Max | Min |
| Torque X-Axis | . | . | . | . |
| Torque Y-Axis | . | . | . | . |
| Torque Z-Axis | . | . | . | . |
| Torque Result | . | . | . | . |

| | 9 G-Level Run LX4314 | | 10 G-Level Run LX4316 | |
|---------------|-------------------------|--------|--------------------------|--------|
| | HIC Nbr | Width | HIC Nbr | Width |
| HIC X-Axis | 40.85 | 81.00 | 51.32 | 79.00 |
| HIC Y-Axis | 0.32 | 131.00 | 0.37 | 162.00 |
| HIC Z-Axis | 3.88 | 54.50 | 6.10 | 55.50 |
| Resultant HIC | 50.76 | 101.50 | 63.92 | 94.00 |



SUBJECT H00136

*** Head Anatomical Configuration ***

Head Mass : 4.235 Kg.

Head Center of Gravity: X = +0.0083 Y = -0.0005 Z = +0.0312 Meters

Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters

Eigenvalues: 1 = +0.02024 2 = +0.02164 3 = +0.01409

| Principal Axis Matrix | | | Moment of inertia matrix in A.C.S. | | |
|-----------------------|----------|----------|------------------------------------|-----------|-----------|
| +0.82900 | +0.00000 | +0.55920 | +0.018316 | +0.000000 | +0.002851 |
| +0.00000 | +1.00000 | +0.00000 | +0.000000 | +0.021640 | +0.000000 |
| -0.55920 | +0.00000 | +0.82900 | +0.002851 | +0.000000 | +0.016012 |

*** Minus X Sled Runs ***

| | | 10 G-Level Run LX3918 | | 12 G-Level Run LX3942 | | 13 G-Level Run LX3953 | | 14 G-Level Run LX3962 | |
|---------------|--------|--------------------------|--------|--------------------------|--------|--------------------------|--------|--------------------------|--------|
| | | Max | Min | Max | Min | Max | Min | Max | Min |
| Force | X-Axis | . | . | . | . | . | . | . | . |
| Force | Y-Axis | . | . | . | . | . | . | . | . |
| Force | Z-Axis | . | . | . | . | . | . | . | . |
| Force | Result | . | . | . | . | . | . | . | . |
| | | 10 G-Level Run LX3918 | | 12 G-Level Run LX3942 | | 13 G-Level Run LX3953 | | 14 G-Level Run LX3962 | |
| | | Max | Min | Max | Min | Max | Min | Max | Min |
| Torque | X-Axis | . | . | . | . | . | . | . | . |
| Torque | Y-Axis | . | . | . | . | . | . | . | . |
| Torque | Z-Axis | . | . | . | . | . | . | . | . |
| Torque | Result | . | . | . | . | . | . | . | . |
| | | 10 G-Level Run LX3918 | | 12 G-Level Run LX3942 | | 13 G-Level Run LX3953 | | 14 G-Level Run LX3962 | |
| | | HIC Nbr | Width | HIC Nbr | Width | HIC Nbr | Width | HIC Nbr | Width |
| HIC | X-Axis | 48.48 | 91.50 | 65.83 | 92.50 | 85.96 | 83.50 | 99.13 | 85.50 |
| HIC | Y-Axis | 0.08 | 528.50 | 0.18 | 189.50 | 0.18 | 194.00 | 0.09 | 84.00 |
| HIC | Z-Axis | 8.95 | 61.00 | 16.22 | 53.50 | 19.11 | 52.00 | 14.07 | 120.00 |
| Resultant HIC | | 65.84 | 107.50 | 95.49 | 95.50 | 121.16 | 100.00 | 128.32 | 85.50 |



SUBJECT H00136

*** Plus Y Sled Runs ***

| | | 5 G-Level | | 6 G-Level | | 7 G-Level | |
|---------------|--------|------------|--------|------------|--------|------------|--------|
| | | Run LX4098 | | Run LX4142 | | Run LX4153 | |
| | | Max | Min | Max | Min | Max | Min |
| HIC | X-Axis | 9.42 | 118.00 | 13.37 | 100.00 | 18.48 | 82.00 |
| HIC | Y-Axis | 0.17 | 188.50 | 0.36 | 154.50 | 0.53 | 127.50 |
| HIC | Z-Axis | 0.77 | 77.50 | 1.28 | 119.00 | 2.64 | 106.50 |
| Resultant HIC | | 11.57 | 124.00 | 16.91 | 104.50 | 24.36 | 90.00 |

***-Minus X / Plus Y ***

| | | 7 G-Level | | 9 G-Level | |
|---------------|--------|------------|--------|------------|--------|
| | | Run LX4247 | | Run LX4263 | |
| | | HIC Nbr | Width | HIC Nbr | Width |
| HIC | X-Axis | 23.27 | 115.00 | 33.30 | 81.50 |
| HIC | Y-Axis | 0.14 | 59.50 | 0.61 | 57.00 |
| HIC | Z-Axis | 1.94 | 58.00 | 6.11 | 63.00 |
| Resultant HIC | | 27.86 | 112.00 | 47.72 | 109.50 |



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